

# **DESIGN CAPACITY TABLES**

for 64 x 41 Lipped Channels

to

# **AS/NZS 4600**

Version 01 June 2019

www.howickltd.com

#### Howick Ltd

Design Capacity Tables for 64 x 41 Lipped Channels to AS/NZS 4600

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Consequently, the information contained in this publication cannot be readily used for coldformed sections produced on machines by other manufacturers, as those sections may vary significantly in geometry and material Standard compliance.

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### **About Howick Ltd**

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Howick Ltd personifies the concept of "Kiwi ingenuity" showcasing technical experties and creativity and that essential "can do" philosophy that underpins the company's world-leading innovation and quality. Given this success, Howick Ltd is often described as producers of "the world's best steel framing machines".

We are a design and manufacturing company with a global philosophy and reach. Our emphasis is on unique research and development and sophisticated design technology enabling cost-effective, efficient end to end construction systems, across a variety of steel framed projects.

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### **Notations & Abbreviations**

Symbol	Description
Ag	gross area of a cross-section
b	flat width of a flange excluding radii
bf	overall width of a flange
Cb	bending coefficient dependent on moment
Cs	coefficient for moment about the cnetroidal axis perpendicular to the symmetry axis
C <sub>TF</sub>	coefficient for unequal end moment
С	distance from the end of a beam to the edge of the bearing force
d	overall depth of a section
<i>d</i> <sub>1</sub>	depth of the flat portion of a web measured along the plane of the web
dL	overall depth of a lip
E	Young's modulus of elasticity
EOF	End One Flange (concentrated load or reaction on a beam)
ETF	End Two Flange (concentrated load or reaction on a beam)
f <sub>u</sub>	minimum tensile strength used in design
fy	minimum yield stress used in design
G	shear modulus of elasticity
l <sub>w</sub>	warping constant for a cross-section
I <sub>x</sub>	second moment of area about the major principal x-axis
l <sub>y</sub>	second moment of area about the minor principal y-axis
IOF	Interior One Flange (concentrated load or reaction on a beam)
ITF	Interior Two Flange (concentrated load or reaction on a beam)
J	torsion constant for the cross-section
L <sub>b</sub>	actual length of bearing
L <sub>e</sub>	effective length of a member
L <sub>ex</sub>	effective length for buckling about the major principal x-axis
L <sub>ey</sub>	effective length for buckling about the minor principal y-axis
L <sub>ez</sub>	effective length for torsional buckling about the longitudinal z-axis
M*	design bending moment

Symbol	Description
M <sub>x</sub> *	design bending moment about the x-axis
<i>M</i> <sub>y</sub> *	design bending moment about the y-axis
M <sub>b</sub>	nominal member moment capacity
M <sub>bdx</sub>	nominal moment capacity about the x-axis for distortional buckling
$M_{ m bdyL}$	nominal moment capacity about the y-axis for distortional buckling (lips in compression)
M <sub>bdyW</sub>	nominal moment capacity about the y-axis for distortional buckling (web in compression)
$M_{ m bx}$	nominal member moment capacity about the x-axis
M <sub>by</sub>	nominal member moment capacity about the y-axis
M <sub>byL</sub>	nominal member moment capacity about the y-axis (lips in compression)
$M_{ m byW}$	nominal member moment capacity about the y-axis (web in compression)
M <sub>sx</sub>	nominal section moment capacity about the x-axis
M <sub>sxf</sub>	nominal yield moment capacity about the x-axis
M <sub>syfL</sub>	nominal yield moment capacity about the y-axis (tension in the lips)
M <sub>syfT</sub>	nominal yield moment capacity about the y-axis (tension in the toes)
M <sub>syfW</sub>	nominal yield moment capacity about the y-axis (tension in the web)
M <sub>syL</sub>	nominal section moment capacity about the y-axis (lips in compression)
M <sub>syT</sub>	nominal section moment capacity about the y-axis (toes in compression)
M <sub>syW</sub>	nominal section moment capacity about the y-axis (web in compression)
My	moment causing initial yield at the extreme compression fibre of a full section
N*	design axial force (tension or compression)
N <sub>c</sub>	nominal member capacity of a member in compression
N <sub>cd</sub>	nominal capacity of a member in compression for distortional buckling
N <sub>ex</sub>	elastic buckling load about the major principal x-axis
N <sub>ey</sub>	elastic buckling load about the minor principal y-axis
Ns	nominal section capacity of a member in compression
Nt	nominal section capacity of a member in tension



Symbol	Description
<i>r</i> i	inside corner radius
<i>r</i> <sub>o1</sub>	polar radius of gyration of the cross-section about the shear centre
r <sub>x</sub>	radius of gyration about the major principal x-axis
ry	radius of gyration about the minor principal y-axis
t	nominal base metal thickness of a section exclusive of coatings
V <sub>vx</sub>	nominal shear capacity of the cross-section perpendicular to the x-axis
V <sub>vy</sub>	nominal shear capacity of the cross-section perpendicular to the x-axis
V <sub>x</sub> *	design shear force
Vy*	design shear force
W <sub>h</sub>	total hole width
X	major principal axis of the cross-section
Xc	co-ordinate of the centroid from the back of the web along the x-axis
xo	co-ordinate of the shear centre from the centroid along the x-axis
у	minor principal axis of the cross-section
Z <sub>x</sub>	elastic section modulus about the major principal x-axis
Z <sub>yL</sub>	elastic section modulus about the minor principal y-axis (lips in compression)
$Z_{yW}$	elastic section modulus about the minor principal y-axis (web in compression)
$\alpha_{T}$	coefficient of thermal expamsion
β <sub>y</sub>	monosymmetry section constant about the y-axis
φ <sub>b</sub>	capacity reduction factor for bending
φ <sub>c</sub>	capacity reduction factor for compression
φ <sub>t</sub>	capacity reduction factor for tension
φv	capacity reduction factor for shear
φw	capacity reduction factor for bearing
ν	Poisson's ratio (= 0.3 for steel)
ρ	density of steel

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### INTRODUCTION

### Scope

These Design Capacity Tables have been prepared for the following nestable lipped channel cold-formed sections manufactured on Howick Ltd. steel roll-forming machines.

64 x 41 x 1.55 LC 64 x 41 x 1.15 LC 64 x 41 x 0.95 LC 64 x 41 x 0.75 LC

The values presented in the tables and graphs are only applicable to sections manufactured on Howick Ltd. machines, and for the specified steel grades complying with AS 1397.

All of the dimensions and section properties required for design are provided, as well as design aids in the form of tables and graphs for members subject to the following design actions:

Bending Axial Compression Axial Tension Combined Actions

These design aids will allow engineers to design most structures without having to refer to the design standard AS/NZS 4600.

### **Design Method**

The Tables and Graphs in this publication have been calculated generally in accordance with the Australian and New Zealand standard AS/NZS 4600 Cold-Formed steel Structures. The Direct Strength Method (DSM) has been used to determine the capacities for axial compression and bending, based on the results of finite strip analyses using the computer program "Thin-Wall" from The University of Sydney.

Where appropriate, the method of calculating capacities in the transition region between local and distortional buckling in accordance with the AISI publication "Direct Strength Mothod" has been used. This is an extension of what is given in AS/NZS 4600.

### Limit States Design

All values presented in these Design Capacity Tables are limit state values in accordance with the Limits State Design requirements of AS/NZS 4600 and AS/NZS 1170.0.

### Units

The units in the Tables are consistent with those in the SI (metric) system. The base units used in the tables and graphs are:

Property	Units	Symbol
Force	Newton	N
Length	metre	m
Mass	kilogram	kg
Stress	Megapascal	MPa

Except for some minor exceptions, all values in the Tables are rounded to three (3) significant figures.

### **Properties of Steel**

The properties of steel used for the calculation of capacities in these Tables are given in the table below. The coefficient of expansion for steel is also listed.

Property	Symbol	Value
Young's Modulus of Elasticity	E	200 x 10 <sup>3</sup> MPa
Shear Modulus	G	80 x 10 <sup>3</sup> MPa
Poisson's Ratio	ν	0.3
Density	ρ	7850 kg/m <sup>3</sup>
Coefficient of Thermal Expansion	ατ	11.7 x 10 <sup>-6</sup> per °C

The steel grades and mechanical properties used for design in accordance with AS/NZS 4600 are given in the table below. Note that the yield stress and tensile strength for thin sections of Grade G550 steel are reduced as required by this standard.

Section	Grade	Yield Stress f <sub>y</sub> (MPa)	Tensile Strength f <sub>u</sub> (MPa)
64 x 41 x 1.55 LC	G450	450	480
64 x 41 x 1.15 LC	G500	500	520
64 x 41 x 0.95 LC	G550	550	550
64 x 41 x 0.75 LC	G550	495	495



### References

**Referenced Standards** 

AS 1397-2011, Continuous hot-dip metallic coated steel sheet and strip - Coatings of zinc and zinc alloyed with aluminium and magnesium, Standards Australia

AS/NZS 1170.1: 2002, Structural Design Actions Part 0: General Principles, Standards Australia.

AS/NZS 4600: 2018, Cold-Formed Steel Structures, Standards Australia.

Other References

AISI 2006, Direct Strength Method (DSM) Design Guide, American Iron and Steel Institute, January 2006.

Centre of Advanced Structural Engineering (CASE) 2001, "THIN-WALL," Computer Program.

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# Part 1: Dimensions & Section Properties

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**DIMENSIONS & SECTION PROPERTIES** 

Table 1.1



		DIMEN	ISIONS					SECTION PROPERTIES											
Designation	Depth	Flange Lip Thick. Width Depth		Inside Corner Radius	Co-ord. of Centroid	of Mass			About x-axis			About	y-axis						
	d	bf	$d_{L}$	t	r <sub>i</sub>	x <sub>c</sub>	mouro	Ag	l <sub>x</sub>	Z <sub>x</sub>	r <sub>x</sub>	l <sub>y</sub>	$Z_{yL}$	$Z_{yW}$	ry				
	mm	mm	mm	mm	mm	mm	kg/m	mm <sup>2</sup>	10 <sup>6</sup> mm <sup>4</sup>	10 <sup>3</sup> mm <sup>3</sup>	mm	10 <sup>6</sup> mm <sup>4</sup>	10 <sup>3</sup> mm <sup>3</sup>	10 <sup>3</sup> mm <sup>3</sup>	mm				
64 x 41 x 1.55 LC - G450	63.5	41.3	10.0	1.55	1.5	15.1	1.90	242	0.163	5.14	26.0	0.0556	2.12	3.68	15.2				
64 x 41 x 1.15 LC - G500	63.5	41.3	10.0	1.15	1.5	15.1	1.43	182	0.124	3.9 <sup>1</sup>	26.2	0.0428	1.64	2.83	15.4				
64 x 41 x 0.95 LC - G550	63.5	41.3	10.0	0.95	1.5	15.1	1.19	151	0.104	3.28	26.3	0.0360	1.38	2.38	15.4				
64 x 41 x 0.75 LC - G550	63.5	41.3	10.0	0.75	1.5	15.1	0.941	120	0.0832	2.62	26.3	0.0290	1.11	1.91	15.5				

NOTES:

1. Calculations of section properties are in accordance with AS/NZS 4600.

2. Thickness refers to the base metal thickness (BMT).

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# SECTION PROPERTIES TO CALCULATE MEMBER STABILITY

Table 1.2



		DIME	INSIO	٩S					RATIOS PROPER					S		MATERIAL		
Designation	Depth	Flange Width	Lip Depth	Thick- ness	Inside Corner Radius	Flat Flat Web Flange Depth Width		Mass <sub>W</sub> per metre	ber vveb	Flange	Shear Centre Co-ord.	Polar Rad. of Gyration about S.C.	Mono- Symmetry Constant	Torsion Constant	Warping Constant	Grade	Design Yield Stress	Design Tensile Strength
	d	bf	$d_{L}$	t	r <sub>i</sub>	d <sub>1</sub>	b	motro	d <sub>1</sub> /t	b/t	x <sub>o</sub>	r <sub>o1</sub>	β <sub>y</sub>	J	l <sub>w</sub>		f <sub>y</sub>	f <sub>u</sub>
	mm	mm	mm	mm	mm	mm	mm	kg/m			mm	mm		mm <sup>4</sup>	10 <sup>6</sup> mm <sup>6</sup>		MPa	MPa
64 x 41 x 1.55 LC - G450	63.5	41.3	10.0	1.55	1.5	57.4	35.2	1.90	37.0	22.7	34.6	45.9	89.1	194	51.1	G450	450	480
64 x 41 x 1.15 LC - G500	63.5	41.3	10.0	1.15	1.5	58.2	36.0	1.43	50.6	31.3	35.1	46.4	90.0	80.1	39.9	G500	500	520
64 x 41 x 0.95 LC - G550	63.5	41.3	10.0	0.95	1.5	58.6	36.4	1.19	61.7	38.3	35.3	46.6	90.4	45.4	33.8	G550	550	550
64 x 41 x 0.75 LC - G550	63.5	41.3	10.0	0.75	1.5	59.0	36.8	0.941	78.7	49.1	35.6	46.9	90.9	22.5	27.4	G550	495	495

#### NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.

2. Thickness refers to the base metal thickness (BMT).

3. Steel grades are in accordance with AS 1397.

4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.

5. The flat flange width is the average of the flanges.

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Graph 2.12: Combined Bending & Bearing (x-axis IOF  $L_b = 150$  mm)

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## MEMBER MOMENT CAPACITY

Members without Full Lateral Restraint

### bending about x-axis

 $C_{\rm b} = 1.0$ 



	Mass	Buckling (	Capacities Design Member Moment Capacity, $\phi_b M_{bx}$ (kNm)														
Designation	per	Local	Distortional														
Designation	metre	$\phi_b M_{sx}$ $\phi_b M_{bdx}$ Effective Length ( $L_e$ ) in metres															
	kg/m	kNm	kNm	0.2	0.3	0.6	0.9	1.2	1.5	1.8	2.1	2.4	2.7	3	3.3	3.6	4
64 x 41 x 1.55 LC - G450	1.90	2.08	1.92	2.01	1.92	1.92	1.92	1.73	1.45	1.13	0.879	0.714	0.598	0.514	0.450	0.400	0.348
64 x 41 x 1.15 LC - G500	1.43	1.71	1.39	1.64	1.39	1.39	1.39	1.39	1.10	0.806	0.614	0.489	0.402	0.340	0.293	0.257	0.220
64 x 41 x 0.95 LC - G550	1.19	1.34	1.14	1.34	1.15	1.14	1.14	1.12	0.918	0.656	0.495	0.390	0.318	0.266	0.227	0.198	0.168
64 x 41 x 0.75 LC - G550	0.941	0.853	0.775	0.853	0.814	0.775	0.775	0.730	0.619	0.492	0.384	0.300	0.242	0.200	0.170	0.146	0.122

NOTES:

- 1. Calculations of section capacities are in accordance with AS/NZS 4600.
- 2. Thickness refers to the base metal thickness (BMT).
- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
- 5. Capacities are calculated for a uniform bending moment ( $C_{\rm b}$  = 1.0).
- 6. Refer to Graph 2.1 for the limits of the local and distortional design moment capacities.
- 7. The effective length  $L_{\rm e} = L_{\rm ey} = L_{\rm ez}$ .







Graph 2.1

# MEMBER MOMENT CAPACITY

Members without Full Lateral Restraint

### bending about x-axis

 $C_{\rm b} = 1.0$ 





#### NOTES:

- 1. Calculations of section capacities are in accordance with AS/NZS 4600.
- 2. Thickness refers to the base metal thickness (BMT).
- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
- 5. Capacities are calculated for a uniform bending moment ( $C_{\rm b}$  = 1.0).
- 6. The effective length  $L_{\rm e} = L_{\rm ev} = L_{\rm ez}$ .





## MEMBER MOMENT CAPACITY

Members without Full Lateral Restraint

bending about y-axis

(Lips in Compression)



	Mass	Buckling	ckling Capacities Design Member Moment Capacity, $\phi_{ m b} M_{ m byL}$ (kNm)														
Designation	per	Local	Distortional														
Designation	metre	$\phi_{\sf b} M_{\sf syL}$	$\phi_{\sf b}  M_{\sf bdyL}$	Effective Length ( $L_{\rm e}$ ) in metres													
	kg/m	kNm	kNm	0.2	0.3	0.6	0.9	1.2	1.5	1.8	2.1	2.4	2.7	3	3.3	3.6	4
64 x 41 x 1.55 LC - G450	1.90	0.860	0.808	0.860	0.808	0.808	0.787	0.679	0.562	0.446	0.365	0.312	0.275	0.248	0.228	0.212	0.196
64 x 41 x 1.15 LC - G500	1.43	0.736	0.593	0.736	0.597	0.593	0.593	0.533	0.396	0.2 <mark>9</mark> 3	0.231	0.190	0.162	0.142	0.127	0.116	0.104
64 x 41 x 0.95 LC - G550	1.19	0.681	0.488	0.668	0.500	0.488	0.488	0.457	0.318	0.231	0.178	0.144	0.121	0.104	0.0917	0.0822	0.0726
64 x 41 x 0.75 LC - G550	0.941	0.490	0.332	0.490	0.360	0.332	0.332	0.332	0.246	0.17 <mark>6</mark>	0.133	0.106	0.0872	0.0737	0.0637	0.0561	0.0485

NOTES:

- 1. Calculations of section capacities are in accordance with AS/NZS 4600.
- 2. Thickness refers to the base metal thickness (BMT).
- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
- 5. Capacities are calculated for  $C_s = 1.0$  and for a uniform bending moment ( $C_{TF} = 1.0$ ).
- 6. Refer to Graph 2.2 for the limits of the local and distortional design moment capacities.
- 7. The effective length  $L_{\rm e} = L_{\rm ex} = L_{\rm ez}$ .

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### Graph 2.2

## MEMBER MOMENT CAPACITY

Members without Full Lateral Restraint

### bending about y-axis







### NOTES:

- 1. Calculations of section capacities are in accordance with AS/NZS 4600.
- 2. Thickness refers to the base metal thickness (BMT).
- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
- 5. Capacities are calculated for  $C_s = 1.0$  and for a uniform bending moment ( $C_{TF} = 1.0$ ).
- 6. The effective length  $L_e = L_{ex} = L_{ez}$ .





## MEMBER MOMENT CAPACITY

Members without Full Lateral Restraint

bending about y-axis

(Web in Compresion)



	Mass	Buckling Capacities						Design N	lember	Moment	Capaci	ty, $\phi_b M_{b}$	<sub>yw</sub> (kNm	)			
Designation	per	Local	Distortional														
Designation	metre	$\phi_{\sf b}  \pmb{M}_{\sf syW}$	$\phi_{b}  M_{bdyW}$		Effective Length ( $L_{e}$ ) in metres												
	kg/m	kNm	kNm	0.2	0.3	0.6	0.9	1.2	1.5	1.8	2.1	2.4	2.7	3	3.3	3.6	4
64 x 41 x 1.55 LC - G450	1.90	0.860	N.A.	0.860	0.860	0.860	0.860	0.860	0.860	0.860	0.860	0.860	0.860	0.860	0.860	0.860	0.860
64 x 41 x 1.15 LC - G500	1.43	0.673	N.A.	0.673	0.673	0.673	0.673	0.673	0.673	0.673	0.673	0.673	0.673	0.673	0.673	0.673	0.673
64 x 41 x 0.95 LC - G550	1.19	0.529	N.A.	0.529	0.529	0.529	0.529	0.529	0.529	0.529	0.529	0.529	0.529	0.529	0.529	0.529	0.529
64 x 41 x 0.75 LC - G550	0.941	0.337	N.A.	0.337	0.337	0.337	0.337	0.337	0.337	0.337	0.337	0.337	0.337	0.337	0.337	0.337	0.337

NOTES:

- 1. Calculations of section capacities are in accordance with AS/NZS 4600.
- 2. Thickness refers to the base metal thickness (BMT).
- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
- 5. Capacities are calculated for  $C_s = 1.0$  and for a uniform bending moment ( $C_{TF} = 1.0$ ).
- 6. Refer to Graph 2.3 for the limits of the local and distortional design moment capacities.
- 7. The effective lengths  $L_{\rm e} = L_{\rm ex} = L_{\rm ez}$ .







Graph 2.3

## MEMBER MOMENT CAPACITY

Members without Full Lateral Restraint

### bending about y-axis



(Web in Compression)



#### NOTES:

- 1. Calculations of section capacities are in accordance with AS/NZS 4600.
- 2. Thickness refers to the base metal thickness (BMT).
- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
- 5. Capacities are calculated for  $C_s = 1.0$  and for a uniform bending moment ( $C_{TF} = 1.0$ ).
- 6. The effective length  $L_e = L_{ex} = L_{ez}$ .



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## **SHEAR CAPACITIES**



	Mass	Shear Capacity						
Designation	per metre	x-axis	y-axis					
	kg/m	φ <sub>v</sub> V <sub>vx</sub> kN	φ <sub>v</sub> V <sub>vy</sub> kN					
64 x 41 x 1.55 LC - G450	1.90	23.1	28.3					
64 x 41 x 1.15 LC - G500	1.43	17.6	23.8					
64 x 41 x 0.95 LC - G550	1.19	12.6	21.9					
64 x 41 x 0.75 LC - G550	0.941	6.22	14.9					

#### NOTES:

- 1. Calculations of section capacities are in accordance with AS/NZS 4600.
- 2. Thickness refers to the base metal thickness (BMT).
- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.

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# WEB BEARING CAPACITY

One Flange Loading or Reaction



Interior Bearing ( $c \ge 1.5 d_1$ )

	Mass		Design Web Bearing Capacity, $\phi_w R_{bx}$ (kN)													
Designation	per	1.5 d <sub>1</sub>			End Bearing	g (c < 1.5 d <sub>1</sub> )			Interior Bearing ( $c \ge 1.5 d_1$ )							
Designation	metre		Bearing Length, $L_{\rm b}$ (mm)							Bearing Length, <i>L</i> <sub>b</sub> (mm)						
	kg/m	mm	25	25 50 75 100 125 150						50	75	100	125	150		
64 x 41 x 1.55 LC - G450	1.90	86.1	6.30	7.83	9.00	10.0	10.9	11.6	14.4	16.5	18.1	19.5	20.7	21.9		
64 x 41 x 1.15 LC - G500	1.43	87.3	4.01	5.04	5.83	6.50	7.09	7.62	8.76	10.2	11.3	12.2	13.0	13.8		
64 x 41 x 0.95 LC - G550	1.19	87.9	3.08	3.90	4.53	5.07	5.53	5.96	6.54	7.67	8.54	9.27	9.92	10.5		
64 x 41 x 0.75 LC - G550	0.941	88.5	1.78	2.27	2.65	2.96	3.24	3.50	3.62	4.29	4.81	5.24	5.62	5.97		

NOTES:

- 1. Calculations of section capacities are in accordance with AS/NZS 4600.
- 2. Thickness refers to the base metal thickness (BMT).
- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.



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## WEB BEARING CAPACITY Two Flange Loading or Reaction



End Bearing ( $c < 1.5 d_1$ )

Interior Bearing ( $c \ge 1.5 d_1$ )

	Mass		Design Web Bearing Capacity, $\phi_w R_{bx}$ (kN)													
Designation	per	1.5 d <sub>1</sub>	End Bearing (c < 1.5 $d_1$ )							Interior Bearing ( $c \ge 1.5 d_1$ )						
Designation	metre				Bearing Len	igth, L <sub>b</sub> (mm)		Bearing Length, <i>L</i> <sub>b</sub> (mm)								
	kg/m	mm	25	50	75	100	125	150	25	50	75	100	125	150		
64 x 41 x 1.55 LC - G450	1.90	86.1	7.87	8.42	8.84	9.19	9.50	9.78	16.1	18.7	20.6	22.2	23.7	24.9		
64 x 41 x 1.15 LC - G500	1.43	87.3	4.33	4.67	4.93	5.15	5.34	5.52	8.70	10.2	11.3	12.3	13.1	13.9		
64 x 41 x 0.95 LC - G550	1.19	87.9	2.99	3.25	3.44	3.60	3.75	3.88	5.80	6.84	7.64	8.32	8.92	9.45		
64 x 41 x 0.75 LC - G550	0.941	88.5	1.48	1.62	1.73	1.82	1.89	1.96	2.62	3.12	3.51	3.83	4.12	4.38		

NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.

2. Thickness refers to the base metal thickness (BMT).

3. Steel grades are in accordance with AS 1397.

4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.

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### Part 3: Members subject to Axial Compression

Table 3.1:Axial Compression CapacityGraph 3.1:Axial Compression Capacity

# Part 3: Members subject to Axial Compression

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# AXIAL COMPRESSION CAPACITY

Table 3.1

 $L_{\rm ex} = L_{\rm ey} = L_{\rm ez}$ 



	Mass	Buckling Capacities		ities Design Axial Compression Capacities, $\phi_c N_c$ (kN)													
Designation	per metre	Local	Distortional														
Designation		Effective Length ( $L_{\rm e}$ ) in metres															
	kg/m	kN	kN	0.2	0.3	0.6	0.9	1.2	1.5	1.8	2.1	2.4	2.7	3	3.3	3.6	4
64 x 41 x 1.55 LC - G450	1.90	86.5	72.3	80.0	80.0	64.8	43.5	27.3	19.0	14.5	11.7	9.92	8.64	7.68	6.95	6.31	5.11
64 x 41 x 1.15 LC - G500	1.43	57.0	49.7	55.4	53.3	43.8	31.9	19.2	12.9	9.5 <mark>3</mark>	7.47	6.12	5.19	4.51	4.01	3.61	3.21
64 x 41 x 0.95 LC - G550	1.19	44.1	39.3	42.7	41.0	33.2	23.4	15.6	10.3	7.50	5.77	4.65	3.88	3.32	2.91	2.59	2.27
64 x 41 x 0.75 LC - G550	0.941	27.6	26.0	26.8	25.9	21.4	15.7	10.9	7.97	5.69	4.31	3.42	2.80	2.36	2.03	1.78	1.53

NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.

2. Thickness refers to the base metal thickness (BMT).

3. Steel grades are in accordance with AS 1397.

4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.

5. Refer to Graph 3.1 for the limits of the local and distortional design moment capacities.

6. The effective length  $L_{e} = L_{ex} = L_{ey} = L_{ez}$ .

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Table 4.1

# **AXIAL TENSION CAPACITIES**

with and without holes



Designation Mass	Mass		Design Axial Tension Capacity, $\phi_t N_t$ (kN)														
	Web Connected							Both Flanges Connected									
Designation	metre	Tension	Tension Total hole Width, <i>w</i> <sub>h</sub> (m)							Total hole Width, <i>w</i> <sub>h</sub> (m)							
	kg/m	(NO Holes)	0	10	20	25	30	35	40	0	10	20	25	30	35	40	
64 x 41 x 1.55 LC - G450	1.90	97.9	75.5	70.6	65.8	63.4	61.0	58.5	56.1	75.5	70.6	65.8	63.4	61.0	58.5	56.1	
64 x 41 x 1.15 LC - G500	1.43	81.7	61.4	57.5	53.6	51.7	49.7	47.8	45.9	61.4	57.5	53.6	51.7	49.7	47.8	45.9	
64 x 41 x 0.95 LC - G550	1.19	74.7	54.0	50.6	47.2	45.5	43.8	42.1	40.4	54.0	50.6	47.2	45.5	43.8	42.1	40.4	
64 x 41 x 0.75 LC - G550	0.941	53.4	38.6	36.2	33.8	32.6	31.4	30.1	28.9	38.6	36.2	33.8	32.6	31.4	30.1	28.9	

NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.

2. Thickness refers to the base metal thickness (BMT).

3. Steel grades are in accordance with AS 1397.

4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.

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#### Part 5: Members subject to Combined Actions

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# Part 5: Members subject to Combined Actions

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# **SECTION & YIELD CAPACITIES**

Table 5.1



	Mass	Design Sectior	Axial Capacities	Design S	Section Moment C	Capacities	Design Yield Moment Capacities (Tension)				
Designation		Tension	Compression	about x-axis	about y-axis		about x-axis	about y-axis			
Designation	per m	$\phi_t N_t$	$\phi_c N_s$	$\phi_b M_{sx}$	φ <sub>b</sub> M <sub>syL</sub> φ <sub>b</sub> M <sub>syW</sub>		$\phi_{\sf b} M_{\sf sxf}$	$\phi_{\sf b} M_{\sf syfL}$	$\phi_{\sf b} M_{\sf syfW}$		
	kg/m	kN	kN	kNm	kNm	kNm	kNm	kNm	kNm		
64 x 41 x 1.55 LC - G450	1.90	97.9	86.5	2.08	0.860	0.860	2.08	0.860	1.49		
64 x 41 x 1.15 LC - G500	1.43	81.7	57.0	1.71	0.736	0.673	1.76	0.736	1.27		
64 x 41 x 0.95 LC - G550	1.19	74.7	44.1	1.34	0.681	0.529	1.62	0.681	1.18		
64 x 41 x 0.75 LC - G550	0.941	53.4	27.6	0.853	0.490	0.337	1.17	0.493	0.852		

NOTES:

- 1. Calculations of section capacities are in accordance with AS/NZS 4600.
- 2. Thickness refers to the base metal thickness (BMT).
- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
- 5.  $\phi_b M_{syL}$  and  $\phi_b M_{syW}$  refer to bending about the y-axis causing compression in the lips and web of the channel respectively.
- φ<sub>b</sub>M<sub>syfL</sub> and φ<sub>b</sub>M<sub>syfW</sub> are the design yield moments for bending about the y-axis causing tension in the lips and web of the channel respectively.
- 7. Capacities are calculated for an equal flange lipped channel using the average flange width.



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Table 5.2

# **ELASTIC BUCKLING LOAD**

buckling about x-axis

q	Mass per						Elast	ic Bucklin	g Load, <i>N</i> e	<sub>x</sub> (kN)					
Designation	metre		Effective Length, $L_{ex}$ (m)												
	kg/m	0.6	1.2	1.5	1.8	2.1	2.4	2.7	3	3.3	3.6	4	4.5	5	6
64 x 41 x 1.55 LC - G450	1.90	895	224	143	99.4	73.0	55.9	44.2	35.8	29.6	24.9	20.1	15.9	12.9	8.95
64 x 41 x 1.15 LC - G500	1.43	681	170	109	75.7	55.6	42.6	33.7	27.3	22.5	18.9	15.3	12.1	9.81	6.81
64 x 41 x 0.95 LC - G550	1.19	570	143	91.3	63.4	46.6	35.6	28.2	22.8	18.9	15.8	12.8	10.1	8.21	5.70
64 x 41 x 0.75 LC - G550	0.941	456	114	73.0	50.7	37.2	28.5	22.5	18.2	15.1	12.7	10.3	8.11	6.57	4.56

NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.

2. Thickness refers to the base metal thickness (BMT).

3. Steel grades are in accordance with AS 1397.

4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.

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Table 5.3

# **ELASTIC BUCKLING LOAD**

buckling about y-axis

	Mass per						Elast	ic Bucklin	g Load, N <sub>e</sub>	<sub>y</sub> (kN)					
Designation	metre			Effective Length, <i>L</i> <sub>ey</sub> (m)											
	kg/m	0.6	1.2	1.5	1.8	2.1	2.4	2.7	3.0	3.3	3.6	4.0	4.5	5.0	6.0
64 x 41 x 1.55 LC - G450	1.90	305	76.2	48.8	33.9	24.9	19.1	15.1	12.2	10.1	8.47	6.86	5.42	4.39	3.05
64 x 41 x 1.15 LC - G500	1.43	235	58.7	37.6	26.1	19.2	14.7	11.6	9.39	7.76	6.52	5.28	4.17	3.38	2.35
64 x 41 x 0.95 LC - G550	1.19	197	49.4	31.6	21.9	16.1	12.3	9.75	7.90	6.53	5.49	4.44	3.51	2.84	1.97
64 x 41 x 0.75 LC - G550	0.941	159	39.7	25.4	17.6	13.0	9.92	7.84	6.35	5.25	4.41	3.57	2.82	2.29	1.59

NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.

2. Thickness refers to the base metal thickness (BMT).

3. Steel grades are in accordance with AS 1397.

4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.

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General

- Table 6.1Dimensions & Section Properties
- Table 6.2 Section Properties to Calculate Member Stability
- Table 6.3: Section & Yield Capacities
- Table 6.4:Axial Compression Capacity
- Graph 6.1: Combined Bending & Shear (bending about y-axis)

# Part 6: MEMBERS with LIPS REMOVED

### GENERAL

When these lipped channel sections are used in frames and trusses, there will be instances where the lips of the sections are removed at the location of the connections. This part of the document provides design tables and graphs which will aid in the design of the unlipoped sections produced by removing the lips. The diagram below illustrates the portion of the section which is removed.

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Table 6.1



## **DIMENSIONS & SECTION PROPERTIES**

Lips Removed



		DIMENSI	ONS				SECTION PROPERTIES								
Designation	Depth	Flange Width	Thickness	Inside Corner Radius	Co-ord. of Centroid	Mass per metre	Gross Section Area		About x-axis		About y-axis				
Ŭ	d	bf	t	r <sub>i</sub>	x <sub>c</sub>	metre	Ag	l <sub>x</sub>	Z <sub>x</sub>	r <sub>x</sub>	l <sub>y</sub>	$Z_{yL}$	$Z_{yW}$	ry	
	mm	mm	mm	mm	mm	kg/m	mm <sup>2</sup>	10 <sup>6</sup> mm <sup>4</sup>	10 <sup>3</sup> mm <sup>3</sup>	mm	10 <sup>6</sup> mm⁴	10 <sup>3</sup> mm <sup>3</sup>	10 <sup>3</sup> mm <sup>3</sup>	mm	
64 x 41 x 1.55 LC-LR - G450	63.5	38.3	1.55	1.5	11.2	1.64	209	0.139	4.39	25.8	0.0317	1.17	2.84	12.3	
64 x 41 x 1.15 LC-LR - G500	63.5	38.7	1.15	1.5	11.2	1.23	157	0.106	3.35	26.0	0.0246	0.897	2.20	12.5	
64 x 41 x 0.95 LC-LR - G550	63.5	38.9	0.95	1.5	11.2	1.03	131	0.0891	2.81	26.1	0.0208	0.752	1.86	12.6	
64 x 41 x 0.75 LC-LR - G550	63.5	39.1	0.75	1.5	11.2	0.815	104	0.0713	2.25	26.2	0.0168	0.603	1.50	12.7	

#### NOTES:

1. Calculations of section properties are in accordance with AS/NZS 4600.

2. Thickness refers to the base metal thickness (BMT).

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Table 6.2



# SECTION PROPERTIES TO CALCULATE MEMBER STABILITY

Lips Removed



	DIMENSIONS									RATIOS PROPERTIES				MATERIAL			
Designation	Depth	Flange Width	Thick- ness	Inside Corner Radius	Flat Web Depth	Flat Flange Width	Mass per metre	Web	Flange	Shear Centre Co-ord.	Polar Rad. of Gyration about S.C.	Mono- Symmetry Constant	Torsion Constant	Warping Constant	Grade	Design Yield Stress	Design Tensile Strength
	d	bf	t	r <sub>i</sub>	d <sub>1</sub>	b	motro	d <sub>1</sub> /t	b/t	x <sub>o</sub>	r <sub>o1</sub>	β <sub>y</sub>	J	I <sub>w</sub>		f <sub>y</sub>	f <sub>u</sub>
	mm	mm	mm	mm	mm	mm	kg/m			mm	mm		mm <sup>4</sup>	10 <sup>6</sup> mm <sup>6</sup>		MPa	MPa
64 x 41 x 1.55 LC-LR - G450	63.5	38.3	1.55	1.5	57.4	35.2	1.64	37.0	22.7	24.9	37.9	79.3	168	21.5	G450	450	480
64 x 41 x 1.15 LC-LR - G500	63.5	38.7	1.15	1.5	58.2	36.0	1.23	50.6	31.3	25.4	38.5	80.2	69.3	16.9	G500	500	520
64 x 41 x 0.95 LC-LR - G550	63.5	38.9	0.95	1.5	58.6	36.4	1.03	61.7	38.3	25.7	38.7	80.7	39.3	14.4	G550	550	550
64 x 41 x 0.75 LC-LR - G550	63.5	39.1	0.75	1.5	59.0	36.8	0.815	78.7	49.1	25.9	39.0	81.2	19.5	11.7	G550	495	495

#### NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.

2. Thickness refers to the base metal thickness (BMT).

3. Steel grades are in accordance with AS 1397.

4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.

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Table 6.3



## **SECTION & YIELD CAPACITIES**

Lips Removed



	Mass	Design Sectior	Axial Capacities	Design S	ection Moment (	Capacities	Design Yield Moment Capacities (Tension)			
Designation		Tension	Compression	about x-axis	about	y-axis	about x-axis	about	y-axis	
Designation	per m	$\phi_t N_t$	$\phi_c N_s$	$\phi_b M_{sx}$	$\phi_{\sf b} M_{\sf syT}$	$\phi_{\sf b} M_{\sf syW}$	$\phi_{\sf b} M_{\sf sxf}$	$\phi_{\sf b} M_{\sf syfT}$	$\phi_{\sf b} M_{\sf syfW}$	
	kg/m	kN	kN	kNm	kNm	kNm	kNm	kNm	kNm	
64 x 41 x 1.55 LC-LR - G450	1.64	84.7	55.8	1.32	0.397	0.475	1.78	0.475	1.15	
64 x 41 x 1.15 LC-LR - G500	1.23	70.8	36.0	0.867	0.263	0.404	1.51	0.404	0.992	
64 x 41 x 0.95 LC-LR - G550	1.03	64.7	27.5	0.668	0.204	0.328	1.39	0.372	0.922	
64 x 41 x 0.75 LC-LR - G550	0.815	46.3	17.1	0.417	0.128	0.209	1.00	0.269	0.670	

NOTES:

- 1. Calculations of section capacities are in accordance with AS/NZS 4600.
- 2. Thickness refers to the base metal thickness (BMT).
- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
- 5.  $\phi_b M_{syT}$  and  $\phi_b M_{syW}$  refer to bending about the y-axis causing compression in the toes and web of the channel respectively.
- 6.  $\phi_b M_{syfT}$  and  $\phi_b M_{syfW}$  are the design yield moment capacities for bending about the y-axis causing tension in the toes and web of the channel respectively.
- 7. All section moment capacities are applicable for unrestrained lengths up to 400 mm. Lips removed WICK 2000 for more than this length is not expected.
- 8. Capacities are calculated for an equal flange channel using the average flange width.





# **AXIAL COMPRESSION CAPACITY**

Table 6.4





	Mass	Desigr	n Axial C	ompress	ion Capa	acity, $\phi_{ m c}$ /	V <sub>c</sub> (kN)	60
Designation	per metre		Effec	ctive Lengtl	n (L <sub>e</sub> ) in m	etres		
	kg/m	0.0	0.10	0.20	0.30	0.35	0.40	50
64 x 41 x 1.55 LC-LR - G450	1.64	55.8	55.3	53.8	51.5	50.1	48.5	
64 x 41 x 1.15 LC-LR - G500	1.23	36.0	35.7	34.6	33.0	32.0	30.9	Ê
64 x 41 x 0.95 LC-LR - G550	1.03	27.5	27.2	26.4	25.1	24.2	23.3	(kNm)
64 x 41 x 0.75 LC-LR - G550	0.815	17.1	16.9	16.5	15.7	15.3	14.7	°, 40 ≥°, 40

#### NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.

2. Thickness refers to the base metal thickness (BMT).

3. Steel grades are in accordance with AS 1397.

- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600.
- 5. Refer to Graph 3.1 for the limits of the local and distortional design moment capacities.

6. The effective length  $L_e = L_{ex} = L_{ey} = L_{ez}$ .





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# Part 7: Wall Framing Design Capacities

## GENERAL

This part of the Design Capacity tables provide capacities which may be used for the design of the sections as wall studs and wall plates. Three typical wall heights are specified for the wall studs.

The NASH wall stud and plate classifications for both Australia and New Zealand are also included in the tables for each section. These are based on the minimum properties and capacities given in the NASH references.

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# Table 7.1 WALL STUD DESIGN CAPACITIES

Unclad



Mass					Design Pro	perties and	Capacities				NA	SH
Designation	per metre		Lateral	Actions		Compr	ession	Tension	Combine	d Actions	Wall Stud Classification	
Dooignation	mene	l <sub>x</sub>	$\phi_{\sf b} M_{\sf sx}$	$\phi_{\rm b}M_{\rm bx}$	$\phi_v V_{vx}$	$\phi_{\rm c} N_{\rm s}$	$\phi_{\rm c} N_{\rm c}$	$\phi_t N_t$	$\phi_{\sf b} M_{\sf sxf}$	N <sub>ex</sub>	Classi	lication
	kg/m	10 <sup>6</sup> mm⁴	kNm	kNm	kN	kN	kN	kN	kNm	kN	Australia	New Zealand
Stud Height 2440 mm												
64 x 41 x 1.55 LC - G450	1.90	0.163	2.08	1.92	23.1	86.5	29.0	75.5	2.08	84.5	SC	SD
64 x 41 x 1.15 LC - G500	1.43	0.124	1.71	1.39	17.6	57.0	21.2	61.4	1.76	64.4	SC	SD
64 x 41 x 0.95 LC - G550	1.19	0.104	1.34	1.14	12.6	44.1	17.4	54.0	1.62	53.9	SC	SC
64 x 41 x 0.75 LC - G550	0.941	0.0832	0.853	0.775	6.22	27.6	11.8	38.6	1.17	43.1	SA	SB
	Stud Height 2740 mm											
64 x 41 x 1.55 LC - G450	1.90	0.163	2.08	1.82	23.1	86.5	23.4	75.5	2.08	67.0	SC	SD
64 x 41 x 1.15 LC - G500	1.43	0.124	1.71	1.39	17.6	57.0	17.0	61.4	1.76	51.1	SC	SB
64 x 41 x 0.95 LC - G550	1.19	0.104	1.34	1.14	12.6	44.1	14.0	54.0	1.62	42.7	SB	SB
64 x 41 x 0.75 LC - G550	0.941	0.0832	0.853	0.762	6.22	27.6	10.2	38.6	1.17	34.2	SA	SB
					Stud	Height 3040	mm					
64 x 41 x 1.55 LC - G450	1.90	0.163	2.08	1.92	23.1	86.5	27.4	75.5	2.08	54.5	SC	SD
64 x 41 x 1.15 LC - G500	1.43	0.124	1.71	1.39	17.6	57.0	20.5	61.4	1.76	41.5	SC	SD
64 x 41 x 0.95 LC - G550	1.19	0.104	1.34	1.14	12.6	44.1	17.1	54.0	1.62	34.7	SC	SC
64 x 41 x 0.75 LC - G550	0.941	0.0832	0.853	0.775	6.22	27.6	11.7	38.6	1.17	27.8	SA	SC



DESIGN CAPACITY TABLES for 64 x 41 Lipped Channels to AS/NZS 4600

#### Wall Stud Design Assumptions

Effective Lengths for Design									
Stud Height (mm)	2440	3040							
No. of Noggings	1	1	2						
L <sub>ex</sub> (mm)	1952	2192	2432						
L <sub>ey</sub> (mm)	976	1096	810						
L <sub>ez</sub> (mm)	976	1096	810						

#### NOTES:

- 1. Noggings are equally spaced.
- 2. Lateral restraint is assumed to be provided by noggings only. Additional lateral restraint provided by cladding is ignored.
- 3. Both flanges of the stud are restrained by the top and bottom plates and the noggings.
- 4. Effective lengths are taken as 80% of the distance between restraints in accordance with NASH Handbook Clause 3.4.2.
- 5. No allowance has been made for holes in the web of the stud.

Symbol	Description
l <sub>x</sub>	second moment of area about the major principal x-axis
$\phi_{\rm c} N_{\rm s}$	design section capacity of a member in compression
$\phi_{c} N_{c}$	design member capacity of a member in compression
$\phi_{\sf b} M_{\sf sx}$	design section moment capacity about the x-axis
$\phi_{\rm b} M_{\rm bx}$	design member moment capacity about the x-axis
$\phi_{\sf b} M_{\sf sxf}$	design yield moment capacity about the x-axis
$\phi_{v} V_{vx}$	design shear capacity of the cross-section perpendicular to the x-axis
N <sub>ex</sub>	elastic buckling load about the major principal x-axis
$\phi_t N_t$	design section capacity of a member in tension
L <sub>ex</sub>	effective length for buckling about the major principal x-axis
L <sub>ey</sub>	effective length for buckling about the minor principal y-axis
L <sub>ez</sub>	effective length for torsional buckling about the longitudinal z-axis

#### References

AS/NZS 4600 Cold-Formed Steel Structures.

NASH Standard (NZ), Residential and Low-Rise Steel Framing, Part 1: Design Criteria.

NASH Standard (Aust.), Residential and Low-Rise Steel Framing, Part 2: Design Solutions. NASH Handbook (Aust.), Best Practice for Design and Construction of Residential and Low-Rise Steel Framing, Chapter 3.

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# Table 7.2 WALL STUD DESIGN CAPACITIES

**Clad Both Sides** 



Mass					Design Pro	perties and	Capacities				NASH	
Designation	per metre		Lateral	Actions		Compr	ession	Tension	Combine	d Actions		Stud
Deelghalleri	metre	l <sub>x</sub>	$\phi_{\rm b} M_{\rm sx}$	$\phi_{\rm b}M_{\rm bx}$	$\phi_{v} V_{vx}$	$\phi_{\rm c} N_{\rm s}$	$\phi_{\rm c} N_{\rm c}$	$\phi_t N_t$	$\phi_{\sf b} M_{\sf sxf}$	N <sub>ex</sub>	Classi	fication
	kg/m	10 <sup>6</sup> mm <sup>4</sup>	kNm	kNm	kN	kN	kN	kN	kNm	kN	Australia	New Zealand
Stud Height 2440 mm												
64 x 41 x 1.55 LC - G450	1.90	0.163	2.08	1.92	23.1	86.5	43.0	75.5	2.08	84.5	SC	SD
64 x 41 x 1.15 LC - G500	1.43	0.124	1.71	1.39	17.6	57.0	32.3	61.4	1.76	64.4	SC	SD
64 x 41 x 0.95 LC - G550	1.19	0.104	1.34	1.14	12.6	44.1	24.0	54.0	1.62	53.9	SC	SC
64 x 41 x 0.75 LC - G550	0.941	0.0832	0.853	0.775	6.22	27.6	16.1	38.6	1.17	43.1	SA	SB
Stud Height 2740 mm												
64 x 41 x 1.55 LC - G450	1.90	0.163	2.08	1.92	23.1	86.5	37.7	75.5	2.08	67.0	SC	SD
64 x 41 x 1.15 LC - G500	1.43	0.124	1.71	1.39	17.6	57.0	28.6	61.4	1.76	51.1	SC	SD
64 x 41 x 0.95 LC - G550	1.19	0.104	1.34	1.14	12.6	44.1	21.5	54.0	1.62	42.7	SC	SC
64 x 41 x 0.75 LC - G550	0.941	0.0832	0.853	0.775	6.22	27.6	14.7	38.6	1.17	34.2	SA	SB
					Stud	Height 3040	mm					
64 x 41 x 1.55 LC - G450	1.90	0.163	2.08	1.92	23.1	86.5	32.4	75.5	2.08	54.5	SC	SD
64 x 41 x 1.15 LC - G500	1.43	0.124	1.71	1.39	17.6	57.0	24.5	61.4	1.76	41.5	SC	SD
64 x 41 x 0.95 LC - G550	1.19	0.104	1.34	1.14	12.6	44.1	19.4	54.0	1.62	34.7	SC	SC
64 x 41 x 0.75 LC - G550	0.941	0.0832	0.853	0.775	6.22	27.6	13.2	38.6	1.17	27.8	SA	SB

DESIGN CAPACITY TABLES for 64 x 41 Lipped Channels to AS/NZS 4600

#### Wall Stud Design Assumptions

Effective Lengths for Design									
Stud Height (mm)	2440	3040							
No. of Noggings	1	1	2						
L <sub>ex</sub> (mm)	1952	2192	2432						
L <sub>ey</sub> (mm)	600	600	600						
L <sub>ez</sub> (mm)	600	600	600						

#### NOTES:

- 1. Noggings are equally spaced.
- 2. Lateral restraint is assumed to be provided the cladding.
- 3. Both flanges of the stud are restrained by the top and bottom plates, the nogging, and the cladding
- 4. Effective length L<sub>ex</sub> is taken as 80% of the ength of the stud in accordance with NASH Handbook Clause 3.4.2.
- 5. Effective lengths  $L_{ey}$  and  $L_{ez}$  are assumed to be as per the table above.
- 6. No allowance has been made for holes in the web of the stud.

Symbol	Description
l <sub>x</sub>	second moment of area about the major principal x-axis
$\phi_{\rm c} N_{\rm s}$	design section capacity of a member in compression
$\phi_{\rm c} N_{\rm c}$	design member capacity of a member in compression
$\phi_{\sf b} M_{\sf sx}$	design section moment capacity about the x-axis
$\phi_{\rm b} M_{\rm bx}$	design member moment capacity about the x-axis
φ <sub>b</sub> M <sub>sxf</sub>	design yield moment capacity about the x-axis
$\phi_{\rm v} V_{\rm vx}$	design shear capacity of the cross-section perpendicular to the x-axis
N <sub>ex</sub>	elastic buckling load about the major principal x-axis
$\phi_t N_t$	design section capacity of a member in tension
L <sub>ex</sub>	effective length for buckling about the major principal x-axis
L <sub>ey</sub>	effective length for buckling about the minor principal y-axis
L <sub>ez</sub>	effective length for torsional buckling about the longitudinal z-axis

#### References

AS/NZS 4600 Cold-Formed Steel Structures.

NASH Standard (NZ), Residential and Low-Rise Steel Framing, Part 1: Design Criteria.

NASH Standard (Aust.), Residential and Low-Rise Steel Framing, Part 2: Design Solutions. NASH Handbook (Aust.), Best Practice for Design and Construction of Residential and Low-Rise Steel Framing, Chapter 3.

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### Table 7.3



## WALL PLATE DESIGN CAPACITIES



Mass per Designation metre	Mass				NASH						
		Full Lipped Char	nnel (at midspan	)	С	hannel Lips Rem	noved (at support	s)	Wall Plate		
Designation	metre	l <sub>y</sub>	$\phi_c N_c$	$\phi_{\rm b}  M_{\rm byL}$	$\phi_{\sf b}  M_{\sf byW}$	$\phi_{c}N_{s}$ $\phi_{b}M_{syT}$ $\phi_{b}M_{syW}$		$\phi_v V_{vy}$	Classi	fication	
	kg/m	10 <sup>6</sup> mm⁴	kN	kNm	kNm	kN	kNm	kNm	kN	Australia	New Zealand
64 x 41 x 1.55 LC - G450	1.90	0.0556	64.8	0.808	0.860	55.8	0.397	0.475	28.3	PC	PE
64 x 41 x 1.15 LC - G500	1.43	0.0428	43.8	0.593	0.673	36.0	0.263	0.404	23.8	PC	PD
64 x 41 x 0.95 LC - G550	1.19	0.0360	33.2	0.488	0.529	27.5	0.204	0.328	21.9	РВ	PC
64 x 41 x 0.75 LC - G550	0.941	0.0290	21.4	0.332	0.337	17.1	0.128	0.209	14.9	PA	PB

#### NOTES:

- 1. The capacities for the full lipped channels are based on an effective length  $L_e = 0.6$  m.
- 2. The capacities of channels with lips removed are section capacities.
- 3. No allowance has been made for holes in the web of the plate in the determination of  $I_{y}$ .
- 4. The NASH Classifications are based on the capacities of the full lipped channels.
- 5. The second moment of area I<sub>v</sub> for the full lipped channel is used for the NASH Australia classification.

	Symbol	Description
	l <sub>y</sub>	second moment of area about the minor principal y-axis
	$\phi_{\rm c} N_{\rm s}$	design section capacity of a member in compression
	$\phi_{\rm c} N_{\rm c}$	design member capacity of a member in compression
n.	$\phi_{\sf b}  \pmb{M}_{\sf byL}$	design section moment capacity about the y-axis (lips in compression)
	$\phi_{\rm b} M_{\rm byW}$	design member moment capacity about the y-axis (web in compression)
	$\phi_{\sf b}  M_{\sf syT}$	design section moment capacity about the y-axis (toes in compression)
wi	φ <sub>b</sub> M <sub>syW</sub>	design section moment capacity about the y-axis (web in compression
VVI	$\phi_{v} V_{vy}$	design shear capacity of the cross-section perpendicular to the y-axis
	L <sub>e</sub>	effective length ( $L_{ex} = L_{ey} = L_{ez}$ )



# Appendix A: SIGNATURE CURVES

## CONTENTS

Appendix A	A: Signature Curves
General	
Graph A.1:	100 x 50 x 1.55 LC - Axial Compression
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Graph A.6:	100 x 50 x 1.15 LC - Bending about x-axis
Graph A.7:	100 x 50 x 1.15 LC - Bending about y-axis (Lips in Compression)
Graph A.8:	100 x 50 x 1.15 LC - Bending about y-axis (Web in Compression)
Graph A.9:	100 x 50 x 0.95 LC - Axial Compression
Graph A.10:	100 x 50 x 0.95 LC - Bending about x-axis
Graph A.11:	100 x 50 x 0.95 LC - Bending about y-axis (Lips in Compression)
Graph A.12:	100 x 50 x 0.95 LC - Bending about y-axis (Web in Compression)
Graph A.13:	100 x 50 x 0.75 LC - Axial Compression
Graph A.14:	100 x 50 x 0.75 LC - Bending about x-axis
Graph A.15:	100 x 50 x 0.75 LC - Bending about y-axis (Lips in Compression)
Graph A.16:	100 x 50 x 0.75 LC - Bending about y-axis (Web in Compression

## GENERAL

This appendix provides the signature curves for each of the sections contained in these Design Capacity Tables. The signature curves were produced in the Thin-Wall buckling analysis program developed by The University of Sydney, and form the basis of design using the Direct Strength Method (DSM). They are included here to provide a clear picture of the buckling behaviour of the sections under the following loading conditions:

axial compression

bending about the x-axis

bending about the y-axis (lips in compression)

bending about the y-axis (web in compression)





































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