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# **DESIGN CAPACITY TABLES**

for 89 x 41 Lipped Channels - Nestable to

# AS/NZS 4600

Version 02 January 2019

www.howickltd.com

#### Howick Ltd

Design Capacity Tables for 89 x 41 Lipped Channels - Nestable to AS/NZS 4600

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#### RELEVANCE OF INFORMATION CONTAINED IN THIS PUBLICATION:

Users of this publication should note that the design capacities, calculations, tabulations and other information contained in this publication are specifically relevant to cold-formed steel sections manufactured on Howick roll-forming machines.

Consequently, the information contained in this publication cannot be readily used for coldformed sections produced on machines by other manufacturers, as those sections may vary significantly in geometry and material Standard compliance.

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## **About Howick Ltd**

Howick Ltd is a well-established and respected, 35 year, family enterprise based in Auckland, New Zealand.

Howick Ltd personifies the concept of "Kiwi ingenuity" showcasing technical experties and creativity and that essential "can do" philosophy that underpins the company's world-leading innovation and quality. Given this success, Howick Ltd is often described as producers of "the world's best steel framing machines".

We are a design and manufacturing company with a global philosophy and reach. Our emphasis is on unique research and development and sophisticated design technology enabling cost-effective, efficient end to end construction systems, across a variety of steel framed projects.

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#### Howick Ltd

117 Vincent Street, Howick Auckland, New Zealand 2014

RE: DESIGN CAPACITY TABLES for 89 x 41 Lipped Channel Nestable to AS/NZS 4600:2018 Version 02 January 2019

#### Att: Nick Coubray,

As requested, Engineering Design Global Enterprise (EDGE Consulting Engineers), has undertaken a peer review of the documentation provided by Howick Ltd for the 89 x 41 Lipped Channel Nestable Sections as manufactured by Howick LTD. EDGE has been provided with the following documents:

- "Howick 89 x 41 LCN - DCT [2] 2018-10-24" and associated calculations.

- "89x41 LCN Properties & Capacities v08.xlsx"
- "89x41 LCN Lips Removed Properties & Capacities v06.xlsx"

These documents have been technically reviewed against the relevant standards.

The design capacity tables provided have been compared to the results within the reviewed spreadsheets and calculations and reviewed in accordance with AS/NZS 4600:2018. All calculations and capacity tables comply with AS/NZS 4600:2018.

Yours faithfully,

Inkt

TIM Peters BEng Meng MIEAust CPEng 67334 RBP RPEQ 5496 MIPENZ MIEPNG © Howick Ltd

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# **Notations & Abbreviations**

Symbol	Description
Ag	gross area of a cross-section
b	flat width of a flange excluding radii
b <sub>f1</sub>	overall width of the larger flange
b <sub>f2</sub>	overall width of the smaller flange
Cb	bending coefficient dependent on moment
Cs	coefficient for moment about the cnetroidal axis perpendicular to the symmetry axis
C <sub>TF</sub>	coefficient for unequal end moment
С	distance from the end of a beam to the edge of the bearing force
d	overall depth of a section
<i>d</i> <sub>1</sub>	depth of the flat portion of a web measured along the plane of the web
dL	overall depth of a lip
E	Young's modulus of elasticity
EOF	End One Flange (concentrated load or reaction on a beam)
ETF	End Two Flange (concentrated load or reaction on a beam)
f <sub>u</sub>	minimum tensile strength used in design
fy	minimum yield stress used in design
G	shear modulus of elasticity
l <sub>w</sub>	warping constant for a cross-section
l <sub>x</sub>	second moment of area about the major principal x-axis
l <sub>y</sub>	second moment of area about the minor principal y-axis
IOF	Interior One Flange (concentrated load or reaction on a beam)
ITF	Interior Two Flange (concentrated load or reaction on a beam)
J	torsion constant for the cross-section
L <sub>b</sub>	actual length of bearing
L <sub>e</sub>	effective length of a member
L <sub>ex</sub>	effective length for buckling about the major principal x-axis
L <sub>ey</sub>	effective length for buckling about the minor principal y-axis
L <sub>ez</sub>	effective length for torsional buckling about the longitudinal z-axis

Symbol	Description
M*	design bending moment
<i>M</i> <sub>x</sub> *	design bending moment about the x-axis
<i>M</i> <sub>y</sub> *	design bending moment about the y-axis
Mb	nominal member moment capacity
<i>M</i> <sub>bdx</sub>	nominal moment capacity about the x-axis for distortional buckling
$M_{ m bdyL}$	nominal moment capacity about the y-axis for distortional buckling (lips in compression)
<i>M</i> <sub>bdyW</sub>	nominal moment capacity about the y-axis for distortional buckling (web in compression)
M <sub>bx</sub>	nominal member moment capacity about the x-axis
M <sub>by</sub>	nominal member moment capacity about the y-axis
M <sub>byL</sub>	nominal member moment capacity about the y-axis (lips in compression)
M <sub>byW</sub>	nominal member moment capacity about the y-axis (web in compression)
M <sub>sx</sub>	nominal section moment capacity about the x-axis
M <sub>sxf</sub>	nominal yield moment capacity about the x-axis
M <sub>syfL</sub>	nominal yield moment capacity about the y-axis (tension in the lips)
M <sub>syfT</sub>	nominal yield moment capacity about the y-axis (tension in the toes)
M <sub>syfW</sub>	nominal yield moment capacity about the y-axis (tension in the web)
M <sub>syL</sub>	nominal section moment capacity about the y-axis (lips in compression)
M <sub>syT</sub>	nominal section moment capacity about the y-axis (toes in compression)
M <sub>syW</sub>	nominal section moment capacity about the y-axis (web in compression)
My	moment causing initial yield at the extreme compression fibre of a full section
N*	design axial force (tension or compression)
N <sub>c</sub>	nominal member capacity of a member in compression
N <sub>cd</sub>	nominal capacity of a member in compression for distortional buckling
N <sub>ex</sub>	elastic buckling load about the major principal x-axis
N <sub>ey</sub>	elastic buckling load about the minor principal y-axis
Ns	nominal section capacity of a member in compression



Symbol	Description
Nt	nominal section capacity of a member in tension
<i>r</i> i	inside corner radius
r <sub>01</sub>	polar radius of gyration of the cross-section about the shear centre
r <sub>x</sub>	radius of gyration about the major principal x-axis
ry	radius of gyration about the minor principal y-axis
t	nominal base metal thickness of a section exclusive of coatings
V <sub>vx</sub>	nominal shear capacity of the cross-section perpendicular to the x-axis
V <sub>vy</sub>	nominal shear capacity of the cross-section perpendicular to the x-axis
V <sub>x</sub> *	design shear force
Vy*	design shear force
W <sub>h</sub>	total hole width
X	major principal axis of the cross-section
Xc	co-ordinate of the centroid from the back of the web along the x-axis
Xo	co-ordinate of the shear centre from the centroid along the x-axis
у	minor principal axis of the cross-section
Z <sub>x</sub>	elastic section modulus about the major principal x-axis
$Z_{\rm yL}$	elastic section modulus about the minor principal y-axis (lips in compression)
Z <sub>yW</sub>	elastic section modulus about the minor principal y-axis (web in compression)
$\alpha_{T}$	coefficient of thermal expamsion
$\beta_y$	monosymmetry section constant about the y-axis
$\phi_{b}$	capacity reduction factor for bending
φc	capacity reduction factor for compression
φt	capacity reduction factor for tension
φ <sub>v</sub>	capacity reduction factor for shear
φw	capacity reduction factor for bearing
ν	Poisson's ratio (= 0.3 for steel)
ρ	density of steel

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## **INTRODUCTION**

#### Scope

These Design Capacity Tables have been prepared for the following nestable lipped channel cold-formed sections manufactured on Howick Ltd. steel roll-forming machines.

89 x 41 x 1.55 LCN 89 x 41 x 1.15 LCN 89 x 41 x 0.95 LCN 89 x 41 x 0.75 LCN

The values presented in the tables and graphs are only applicable to sections manufactured on Howick Ltd. machines, and for the specified steel grades complying with AS 1397.

All of the dimensions and section properties required for design are provided, as well as design aids in the form of tables and graphs for members subject to the following design actions:

Bending Axial Compression Axial Tension Combined Actions

These design aids will allow engineers to design most structures without having to refer to the design standard AS/NZS 4600.

#### **Design Method**

The Tables and Graphs in this publication have been calculated generally in accordance with the Australian and New Zealand standard AS/NZS 4600 Cold-Formed steel Structures. The Direct Strength Method (DSM) has been used to determine the capacities for axial compression and bending, based on the results of finite strip analyses using the computer program "Thin-Wall" from The University of Sydney.

Where appropriate, the method of calculating capacities in the transition region between local and distortional buckling in accordance with the AISI publication "Direct Strength Mothod" has been used. This is an extension of what is given in AS/NZS 4600.

#### Limit States Design

All values presented in these Design Capacity Tables are limit state values in accordance with the Limits State Design requirements of AS/NZS 4600 and AS/NZS 1170.0.

#### Units

The units in the Tables are consistent with those in the SI (metric) system. The base units used in the tables and graphs are:

Property	Units	Symbol
Force	Newton	Ν
Length	metre	m
Mass	kilogram	kg
Stress	Megapascal	MPa

Except for some minor exceptions, all values in the Tables are rounded to three (3) significant figures.

#### **Properties of Steel**

The properties of steel used for the calculation of capacities in these Tables are given in the table below. The coefficient of expansion for steel is also listed.

Property	Symbol	Value
Young's Modulus of Elasticity	Е	200 x 10 <sup>3</sup> MPa
Shear Modulus	G	80 x 10 <sup>3</sup> MPa
Poisson's Ratio	ν	0.3
Density	ρ	7850 kg/m <sup>3</sup>
Coefficient of Thermal Expansion	ατ	11.7 x 10 <sup>-6</sup> per °C

The steel grades and mechanical properties used for design in accordance with AS/NZS 4600 are given in the table below. Note that the yield stress and tensile strength for thin sections of Grade G550 steel are reduced as required by this standard.

Section	Grade	Yield Stress f <sub>y</sub> (MPa)	Tensile Strength f <sub>u</sub> (MPa)
89 x 41 x 1.55 LCN	G450	450	480
89 x 41 x 1.15 LCN	G500	500	520
89 x 41 x 0.95 LCN	G550	550	550
89 x 41 x 0.75 LCN	G550	495	495



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## References

#### **Referenced Standards**

AS 1397-2011, Continuous hot-dip metallic coated steel sheet and strip - Coatings of zinc and zinc alloyed with aluminium and magnesium, Standards Australia

AS/NZS 1170.1: 2002, Structural Design Actions Part 0: General Principles, Standards Australia.

AS/NZS 4600: 2018, Cold-Formed Steel Structures, Standards Australia.

**Other References** 

AISI 2006, Direct Strength Method (DSM) Design Guide, American Iron and Steel Institute, January 2006.

Centre of Advanced Structural Engineering (CASE) 2001, "THIN-WALL," Computer Program.

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 Dimensions & Section Properties

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# Part 1: Dimensions & Section Properties

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# **DIMENSIONS & SECTION PROPERTIES**



		DI	MENSIC	NS					SECTION PROPERTIES										
Designation	Depth	LargeSmallLipInsideCo-ord.GrossFlangeFlangeDepthThick.CornerofMassSectionAbout x-axisWidthWidthDepthRadiusCentroidper metreArea								About	y-axis								
	d	b <sub>f1</sub>	b <sub>f2</sub>	$d_{L}$	t	<i>r</i> i	xc	mouo	Ag	l <sub>x</sub>	Z <sub>x</sub>	r <sub>x</sub>	l <sub>y</sub>	$Z_{\rm yL}$	$Z_{yW}$	ry			
	mm	mm	mm	mm	mm	mm	mm	kg/m	mm <sup>2</sup>	10 <sup>6</sup> mm <sup>4</sup>	10 <sup>3</sup> mm <sup>3</sup>	mm	10 <sup>6</sup> mm <sup>4</sup>	10 <sup>3</sup> mm <sup>3</sup>	10 <sup>3</sup> mm <sup>3</sup>	mm			
89 x 41 x 1.55 LCN - G450	89.0	41.3	39.0	10.0	1.55	1.5	12.6	2.18	278	0.347	7.81	35.4	0.0584	2.12	4.62	14.5			
89 x 41 x 1.15 LCN - G500	89.0	41.3	39.0	10.0	1.15	1.5	12.6	1.64	208	0.264	5.92	35.6	0.0450	1.63	3.55	14.7			
89 x 41 x 0.95 LCN - G550	89.0	41.3	39.0	10.0	0.95	1.5	12.6	1.36	173	0.220	4.95	35.7	0.0378	1.38	2.99	14.8			
89 x 41 x 0.75 LCN - G550	89.0	41.3	39.0	10.0	0.75	1.5	12.7	1.08	137	0.176	3.95	35.8	0.0304	1.11	2.40	14.9			

NOTES:

1. Calculations of section properties are in accordance with AS/NZS 4600.

2. Thickness refers to the base metal thickness (BMT).

3. Properties are calculated for an equal flange lipped channel using the average flange width.

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# SECTION PROPERTIES TO CALCULATE MEMBER STABILITY



	DIMENSIONS										RATIOS PROPERTIES							MATERIAL		
Designation	Depth	Large Flange Width	Small Flange Width	Lip Depth	Thick- ness	Inside Corner Radius	Flat Web Depth	Flat Flange Width	Mass per metre	Web	Flange	Shear Centre Co-ord.	Polar Rad. of Gyration about S.C.		Torsion Constant	Warping Constant	Grade	Yield	Design Tensile Strength	
	d	b <sub>f1</sub>	b <sub>f2</sub>	$d_{L}$	t	r <sub>i</sub>	d <sub>1</sub>	b	motro	d <sub>1</sub> /t	b/t	x <sub>o</sub>	r <sub>o1</sub>	β <sub>y</sub>	J	I <sub>w</sub>		f <sub>y</sub>	f <sub>u</sub>	
	mm	mm	mm	mm	mm	mm	mm	mm	kg/m			mm	mm		mm <sup>4</sup>	10 <sup>6</sup> mm <sup>6</sup>		MPa	MPa	
89 x 41 x 1.55 LCN - G450	89.0	41.3	39.0	10.0	1.55	1.5	82.9	34.1	2.18	53.5	22.0	30.1	48.7	101	222	96.0	G450	450	480	
89 x 41 x 1.15 LCN - G500	89.0	41.3	39.0	10.0	1.15	1.5	83.7	34.9	1.64	72.8	30.3	30.6	49.1	101	91.8	74.6	G500	500	520	
89 x 41 x 0.95 LCN - G550	89.0	41.3	39.0	10.0	0.95	1.5	84.1	35.3	1.36	88.5	37.1	30.8	49.4	102	52.0	63.1	G550	550	550	
89 x 41 x 0.75 LCN - G550	89.0	41.3	39.0	10.0	0.75	1.5	84.5	35.7	1.08	113	47.5	31.0	49.6	102	25.7	50.9	G550	495	495	

NOTES:

- 1. Calculations of section capacities are in accordance with AS/NZS 4600.
- 2. Thickness refers to the base metal thickness (BMT).
- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
- 5. The flat flange width is the average of the flanges.
- 6. Properties are calculated for an equal flange lipped channel using the average flange width.





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# Part 2: MEMBERS SUBJECT TO BENDING

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#### Part 2: Members subject to Bending

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0 1 0 10	

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## Table 2.1

# **MEMBER MOMENT CAPACITY**

Members without Full Lateral Restraint

bending about x-axis

 $C_{\rm b} = 1.0$ 



Mass	Buckling (					Design	Member	Momen	it Capac	ity, $\phi_{ m b}M_{ m b}$	<sub>ox</sub> (kNm)						
Designation	per	Local	Distortional														
Designation	metre	$\phi_{\sf b} M_{\sf sx}$	$\phi_{\rm b}  M_{\rm bdx}$						Effec	Effective Length ( $L_{e}$ ) in metres							
	kg/m	kNm	kNm	0.2	0.3	0.6	0.9	1.2	1.5	1.8	2.1	2.4	2.7	3	3.3	3.6	4
89 x 41 x 1.55 LCN - G450	2.18	3.16	2.81	2.96	2.81	2.81	2.81	2.52	2.01	1.48	1.13	0.907	0.749	0.635	0.549	0.483	0.416
89 x 41 x 1.15 LCN - G500	1.64	2.56	2.03	2.39	2.03	2.03	2.03	2.02	1.52	1.08	0.815	0.641	0.521	0.435	0.371	0.322	0.273
89 x 41 x 0.95 LCN - G550	1.36	2.01	1.65	2.01	1.66	1.65	1.65	1.62	1.26	0.892	0.667	0.520	0.420	0.348	0.294	0.253	0.212
89 x 41 x 0.75 LCN - G550	1.08	1.27	1.12	1.27	1.17	1.12	1.12	1.07	0.878	0.690	0.524	0.406	0.325	0.267	0.225	0.192	0.159

NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.

2. Thickness refers to the base metal thickness (BMT).

- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
- 5. Capacities are calculated for a uniform bending moment ( $C_{\rm b}$  = 1.0).
- 6. Refer to Graph 2.1 for the limits of the local and distortional design moment capacities.
- 7. The effective length  $L_{\rm e} = L_{\rm ey} = L_{\rm ez}$ .
- 8. Capacities are calculated for an equal flange lipped channel using the average flange width. HOWICK Ltd



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Graph 2.1

# MEMBER MOMENT CAPACITY



Members without Full Lateral Restraint

#### bending about x-axis

 $C_{\rm b} = 1.0$ 



#### NOTES:

- 1. Calculations of section capacities are in accordance with AS/NZS 4600.
- 2. Thickness refers to the base metal thickness (BMT).
- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
- 5. Capacities are calculated for a uniform bending moment ( $C_{\rm b}$  = 1.0).
- 6. The effective length  $L_{\rm e} = L_{\rm ey} = L_{\rm ez}$ .
- 7. Capacities are calculated for an equal flange lipped channel using the average flange width.



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# $t \rightarrow b_{f1}$

## Table 2.2

# MEMBER MOMENT CAPACITY

Members without Full Lateral Restraint

bending about y-axis

(Lips in Compression)



Tension

	Mass	Buckling	uckling Capacities Design Member Moment Capacity, $\phi_b M_{byL}$ (kNm)														
Designation	per	Local	Distortional														
Designation	metre	$\phi_{\rm b} M_{\rm syL}$	$\phi_{\sf b} M_{\sf bdyL}$		Effective Length (L <sub>e</sub> ) in metres												
	kg/m	kNm	kNm	0.2	0.3	0.6	0.9	1.2	1.5	1.8	2.1	2.4	2.7	3.0	3.3	3.6	4.0
89 x 41 x 1.55 LCN - G450	2.18	0.860	0.804	0.860	0.804	0.804	0.804	0.780	0.697	0.609	0.520	0.436	0.375	0.332	0.299	0.274	0.249
89 x 41 x 1.15 LCN - G500	1.64	0.736	0.590	0.736	0.594	0.590	0.590	0.590	0.551	0.450	0.351	0.283	0.236	0.203	0.178	0.159	0.140
89 x 41 x 0.95 LCN - G550	1.36	0.681	0.486	0.681	0.511	0.486	0.486	0.486	0.477	0.366	0.278	0.221	0.182	0.154	0.133	0.117	0.102
89 x 41 x 0.75 LCN - G550	1.08	0.483	0.330	0.483	0.372	0.330	0.330	0.330	0.330	0.283	0.213	0.167	0.136	0.113	0.0964	0.0838	0.0711

NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.

- 2. Thickness refers to the base metal thickness (BMT).
- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
- 5. Capacities are calculated for  $C_s = 1.0$  and for a uniform bending moment ( $C_{TF} = 1.0$ ).
- 6. Refer to Graph 2.2 for the limits of the local and distortional design moment capacities.
- 7. The effective length  $L_{\rm e} = L_{\rm ex} = L_{\rm ez}$ .
- 8. Capacities are calculated for an equal flange lipped channel using the average flange width.





# Graph 2.2

# MEMBER MOMENT CAPACITY

Members without Full Lateral Restraint

#### bending about y-axis

(Lips in Compression)







#### NOTES:

- 1. Calculations of section capacities are in accordance with AS/NZS 4600.
- 2. Thickness refers to the base metal thickness (BMT).
- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
- 5. Capacities are calculated for  $C_s = 1.0$  and for a uniform bending moment ( $C_{TF} = 1.0$ ).
- 6. The effective length  $L_{e} = L_{ex} = L_{ez}$ .
- 7. Capacities are calculated for an equal flange lipped channel using the average flange width.



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# $t \rightarrow b_{f_2}$

## Table 2.3

# MEMBER MOMENT CAPACITY

Members without Full Lateral Restraint

bending about y-axis

(Web in Compresion)



	Mass	Buckling (	Design Member Moment Capacity, $\phi_b M_{byW}$ (kNm)														
Designation	per	Local	Distortional														
Designation	metre	$\phi_{\sf b} M_{\sf syW}$	$\phi_{\rm b}  M_{ m bdyW}$	Effective Length ( $L_{e}$ ) in metres													
	kg/m	kNm	kNm	0.2	0.3	0.6	0.9	1.2	1.5	1.8	2.1	2.4	2.7	3.0	3.3	3.6	4.0
89 x 41 x 1.55 LCN - G450	2.18	0.846	N.A.	0.846	0.846	0.846	0.846	0.846	0.846	0.846	0.846	0.846	0.846	0.846	0.846	0.846	0.846
89 x 41 x 1.15 LCN - G500	1.64	0.574	N.A.	0.574	0.574	0.574	0.574	0.574	0.574	0.574	0.574	0.574	0.574	0.574	0.574	0.574	0.574
89 x 41 x 0.95 LCN - G550	1.36	0.450	N.A.	0.450	0.450	0.450	0.450	0.450	0.450	0.450	0.450	0.450	0.450	0.450	0.450	0.450	0.450
89 x 41 x 0.75 LCN - G550	1.08	0.286	N.A.	0.286	0.286	0.286	0.286	0.286	0.286	0.286	0.286	0.286	0.286	0.286	0.286	0.286	0.286

NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.

- 2. Thickness refers to the base metal thickness (BMT).
- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
- 5. Capacities are calculated for  $C_s = 1.0$  and for a uniform bending moment ( $C_{TF} = 1.0$ ).
- 6. Refer to Graph 2.3 for the limits of the local and distortional design moment capacities.
- 7. The effective lengths  $L_e = L_{ex} = L_{ez}$ .
- 8. Capacities are calculated for an equal flange lipped channel using the average flange width.



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Graph 2.3

# MEMBER MOMENT CAPACITY

Members without Full Lateral Restraint

#### bending about y-axis

(Web in Compression)







- 1. Calculations of section capacities are in accordance with AS/NZS 4600.
- 2. Thickness refers to the base metal thickness (BMT).
- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
- 5. Capacities are calculated for  $C_s = 1.0$  and for a uniform bending moment ( $C_{TF} = 1.0$ ).
- 6. The effective length  $L_{e} = L_{ex} = L_{ez}$ .
- 7. Capacities are calculated for an equal flange lipped channel using the average flange width.



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## Table 2.4

# **SHEAR CAPACITIES**



	Mass	Shear Capacity					
Designation	per	x-axis	y-axis				
Doolghadon	metre	$\phi_{v} V_{vx}$	$\phi_v V_{vy}$				
	kg/m	kN	kN				
89 x 41 x 1.55 LCN - G450	2.18	30.3	27.4				
89 x 41 x 1.15 LCN - G500	1.64	15.8	23.1				
89 x 41 x 0.95 LCN - G550	1.36	8.87	21.2				
89 x 41 x 0.75 LCN - G550	1.08	4.34	14.9				

#### NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.

- 2. Thickness refers to the base metal thickness (BMT).
- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
- 5. Capacities are calculated for an equal flange lipped channel using the average flange width.

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# Graph 2.4

# **COMBINED BENDING & SHEAR** bending about x-axis





#### NOTES:

- 1. Calculations of section capacities are in accordance with AS/NZS 4600.
- 2. Thickness refers to the base metal thickness (BMT).
- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
- 5. Capacities are calculated for an equal flange lipped channel using the average flange width.



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# **COMBINED BENDING & SHEAR**

**bending about y-axis** (Lips in Compression)

Graph 2.5





30 25 20 15 10 89 x 41 x 1.55 LCN - G450 89 x 41 x 1.15 LCN - G500 89 x 41 x 0.95 LCN - G550 89 x 41 x 0.95 LCN - G550

#### NOTES:

- 1. Calculations of section capacities are in accordance with AS/NZS 4600.
- 2. Thickness refers to the base metal thickness (BMT).
- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
- 5. Capacities are calculated for an equal flange lipped channel using the average flange width.



0.1

0.2

0.3

0.4

0.5

Design Bending Moment  $M_v^*$  (kNm)

0.6

Design Shear Force  $V_y^*$  (kN)

5

0 0

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0.7

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0.8

0.9



# **COMBINED BENDING & SHEAR**

bending about y-axis (Web in Compression)

Graph 2.6







- 1. Calculations of section capacities are in accordance with AS/NZS 4600.
- 2. Thickness refers to the base metal thickness (BMT).
- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
- 5. Capacities are calculated for an equal flange lipped channel using the average flange width.



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## Table 2.5

# WEB BEARING CAPACITY

One Flange Loading or Reaction



End Bearing ( $c < 1.5 d_1$ )

Interior Bearing ( $c \ge 1.5 d_1$ )

Designation	Mass		Design Web Bearing Capacity, $\phi_w R_{bx}$ (kN)											
	per	1.5 d <sub>1</sub>			End Bearing			Interior Bearing ( $c \ge 1.5 d_1$ )						
	metre				Bearing Len	gth, <i>L</i> <sub>b</sub> (mm)					Bearing Len	igth, <i>L</i> <sub>b</sub> (mm)		
	kg/m	mm	25	50	75	100	125	150	25	50	75	100	125	150
89 x 41 x 1.55 LCN - G450	2.18	124.4	6.13	7.61	8.75	9.71	10.6	11.3	14.2	16.3	17.9	19.3	20.5	21.6
89 x 41 x 1.15 LCN - G500	1.64	125.6	3.88	4.88	5.64	6.29	6.85	7.37	8.62	10.0	11.1	12.0	12.8	13.6
89 x 41 x 0.95 LCN - G550	1.36	126.2	2.97	3.76	4.37	4.88	5.33	5.74	6.43	7.54	8.39	9.11	9.75	10.3
89 x 41 x 0.75 LCN - G550	1.08	126.8	1.70	2.17	2.53	2.84	3.11	3.35	3.5 <mark>5</mark>	4.21	4.72	5.14	5.52	5.85

NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.

2. Thickness refers to the base metal thickness (BMT).

- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.

5. Capacities are calculated for an equal flange lipped channel using the average flange width.



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## Table 2.6

# WEB BEARING CAPACITY

Two Flange Loading or Reaction



Designation metre	Mass		Design Web Bearing Capacity, $\phi_w R_{bx}$ (kN)												
	per	1.5 d <sub>1</sub>			End Bearin	g (c < 1.5 d <sub>1</sub> )			Interior Bearing ( $c \ge 1.5 d_1$ )						
	metre				Bearing Ler	igth, L <sub>b</sub> (mm)					Bearing Len	gth, <i>L</i> <sub>b</sub> (mm)			
	mm	25	50	75	100	125	150	25	50	75	100	125	150		
89 x 41 x 1.55 LCN - G450	2.18	124.4	7.36	7.87	8.26	8.59	8.89	9.15	16.1	18.6	20.6	22.2	23.6	24.9	
89 x 41 x 1.15 LCN - G500	1.64	125.6	3.99	4.30	4.54	4.74	4.92	5.08	8.69	10.2	11.3	12.3	13.1	13.9	
89 x 41 x 0.95 LCN - G550	1.36	126.2	2.72	2.95	3.13	3.28	3.41	3.53	5.79	6.83	7.63	8.31	8.90	9.44	
89 x 41 x 0.75 LCN - G550	1.08	126.8	1.32	1.45	1.54	1.62	1.69	1.75	2.61	3.11	3.50	3.82	4.11	4.37	

NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.

2. Thickness refers to the base metal thickness (BMT).

3. Steel grades are in accordance with AS 1397.

4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.

5. Capacities are calculated for an equal flange lipped channel using the average flange width.

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#### Part 3: Members subject to Axial Compression

Table 3.1:Axial Compression CapacityGraph 3.1:Axial Compression Capacity

# Part 3: Members subject to Axial Compression

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# AXIAL COMPRESSION CAPACITY

Table 3.1

 $L_{\rm ex} = L_{\rm ey} = L_{\rm ez}$ 



Designation	Mass	Buckling (	Capacities	Design Axial Compression Capacities, $\phi_c N_c$ (kN)													
	per	Local	Distortional														
Doorgination	metre	$\phi_{\rm c} N_{\rm s}$	$\phi_{\rm c} N_{\rm cd}$		Effective Length ( $L_{e}$ ) in metres												
	kg/m	kN	kN	0.2	0.3	0.6	0.9	1.2	1.5	1.8	2.1	2.4	2.7	3.0	3.3	3.6	4.0
89 x 41 x 1.55 LCN - G450	2.18	80.4	74.7	78.9	77.2	68.6	56.9	44.3	30.3	22.6	17.9	14.8	11.8	9.55	7.89	6.63	5.37
89 x 41 x 1.15 LCN - G500	1.64	52.3	50.4	51.3	50.1	44.1	35.8	26.9	20.4	15.4	11.9	9.55	7.96	6.82	5.98	5.10	4.13
89 x 41 x 0.95 LCN - G550	1.36	40.2	39.5	39.4	38.4	33.4	26.6	19.5	14.7	11.7	9.37	7.44	6.11	5.17	4.46	3.93	3.39
89 x 41 x 0.75 LCN - G550	1.08	25.1	25.9	24.6	24.0	21.2	17.3	13.0	9.83	7.82	6.44	5.46	4.54	3.78	3.22	2.79	2.37

NOTES:

- 1. Calculations of section capacities are in accordance with AS/NZS 4600.
- 2. Thickness refers to the base metal thickness (BMT).
- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
- 5. Refer to Graph 3.1 for the limits of the local and distortional design moment capacities.
- 6. The effective length  $L_{e} = L_{ex} = L_{ey} = L_{ez}$ .
- 7. Capacities are calculated for an equal flange lipped channel using the average flange width.



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# Part 4: Members subject to Axial Tension

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Part 4: Members subject to Axial Tension

 Table 4.1:
 Axial Tension Capacity



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Table 4.1

# **AXIAL TENSION CAPACITIES**

with and without holes



Designation Mass metre	Mass						Design /	Axial Tens	ion Capa	city, $\phi_t N_t$	(kN)					
		Uniform	Web Connected							Both Flanges Connected						
	Tension	Total hole Width, $w_h$ (m)							Total hole Width, w <sub>h</sub> (m)							
	kg/m	kg/m (NO Holes)	0	10	20	25	30	35	40	0	10	20	25	30	35	40
89 x 41 x 1.55 LCN - G450	2.18	112.5	86.7	81.9	77.0	74.6	72.2	69.8	67.3	86.7	81.9	77.0	74.6	72.2	69.8	67.3
89 x 41 x 1.15 LCN - G500	1.64	93.7	70.4	66.5	62.7	60.7	58.8	56.8	54.9	70.4	66.5	62.7	60.7	58.8	56.8	54.9
89 x 41 x 0.95 LCN - G550	1.36	85.6	61.9	58.5	55.1	53.4	51.7	50.0	48.3	61.9	58.5	55.1	53.4	51.7	50.0	48.3
89 x 41 x 0.75 LCN - G550	1.08	61.2	44.2	41.8	39.4	38.2	37.0	35.7	34.5	44.2	41.8	39.4	38.2	37.0	35.7	34.5

NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.

2. Thickness refers to the base metal thickness (BMT).

3. Steel grades are in accordance with AS 1397.

4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.

5. Capacities are calculated for an equal flange lipped channel using the average flange width.

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#### Part 5: Members subject to Combined Actions

Table 5.1:	Section & Yield Capacities
Table 5.2:	Elastic Buckling Load (x-axis)
Table 5.3:	Elastic Buckling Load (y-axis)

# Part 5: Members subject to Combined Actions

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# **SECTION & YIELD CAPACITIES**

Table 5.1



Designation	Mass	Design Sectior	Axial Capacities	Design S	Section Moment C	capacities	Design Yield Moment Capacities (Tension)			
	made	Tension	Compression	about x-axis	about	y-axis	about x-axis	y-axis		
Designation	per m	$\phi_t N_t$	$\phi_c N_s$	φ <sub>c</sub> N <sub>s</sub> φ <sub>b</sub> M <sub>sx</sub>		$\phi_b M_{syL} \qquad \phi_b M_{syW}$		$\phi_{\rm b}M_{\rm syfL}$	$\phi_{\sf b} M_{\sf syfW}$	
	kg/m	kN	kN	kNm	kNm	kNm	kNm	kNm	kNm	
89 x 41 x 1.55 LCN - G450	2.18	112	80.4	3.16	0.860	0.846	3.16	0.860	1.87	
89 x 41 x 1.15 LCN - G500	1.64	93.7	52.3	2.56	0.736	0.574	2.67	0.736	1.60	
89 x 41 x 0.95 LCN - G550	1.36	85.6	40.2	2.01	0.681	0.450	2.45	0.681	1.48	
89 x 41 x 0.75 LCN - G550	1.08	61.2	25.1	1.27	0.483	0.286	1.76	0.493	1.07	

NOTES:

- 1. Calculations of section capacities are in accordance with AS/NZS 4600.
- 2. Thickness refers to the base metal thickness (BMT).
- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
- 5.  $\phi_b M_{syL}$  and  $\phi_b M_{syW}$  refer to bending about the y-axis causing compression in the lips and web of the channel respectively.
- φ<sub>b</sub>M<sub>syfL</sub> and φ<sub>b</sub>M<sub>syfW</sub> are the design yield moments for bending about the y-axis causing tension in the lips and web of the channel respectively.
- 7. Capacities are calculated for an equal flange lipped channel using the average flange width.




Table 5.2

## **ELASTIC BUCKLING LOAD**

buckling about x-axis

	Mass per						Elast	ic Bucklin	g Load, <i>N</i> e	<sub>ex</sub> (kN)					
Designation	metre		Effective Length, L <sub>ex</sub> (m)												
	kg/m	0.2	0.3	0.6	0.9	1.2	1.5	1.8	2.1	2.4	2.7	3.0	3.3	3.6	4.0
89 x 41 x 1.55 LCN - G450	2.18	17147	7621	1905	847	476	305	212	156	119	94.1	76.2	63.0	52.9	42.9
89 x 41 x 1.15 LCN - G500	1.64	13006	5781	1445	642	361	231	161	118	90.3	71.4	57.8	47.8	40.1	32.5
89 x 41 x 0.95 LCN - G550	1.36	10863	4828	1207	536	302	193	134	98.5	75.4	59.6	48.3	39.9	33.5	27.2
89 x 41 x 0.75 LCN - G550	1.08	8670	3853	963	428	241	154	107	78.6	60.2	47.6	38.5	31.8	26.8	21.7

NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.

2. Thickness refers to the base metal thickness (BMT).

- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
- 5. Capacities are calculated for an equal flange lipped channel using the average flange width.

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Table 5.3

## **ELASTIC BUCKLING LOAD**

buckling about y-axis

	Mass per						Elast	ic Bucklin	g Load, <i>N</i> e	<sub>y</sub> (kN)					
Designation	metre		Effective Length, $L_{ey}$ (m)												
	kg/m	0.2	0.3	0.6	0.9	1.2	1.5	1.8	2.1	2.4	2.7	3.0	3.3	3.6	4.0
89 x 41 x 1.55 LCN - G450	2.18	2882	1281	320	142	80.1	51.2	35.6	26.1	20.0	15.8	12.8	10.6	8.89	7.20
89 x 41 x 1.15 LCN - G500	1.64	2218	986	246	110	61.6	39.4	27.4	20.1	15.4	12.2	9.86	8.15	6.85	5.55
89 x 41 x 0.95 LCN - G550	1.36	1866	830	207	92.2	51.8	33.2	23.0	16.9	13.0	10.2	8.30	6.86	5.76	4.67
89 x 41 x 0.75 LCN - G550	1.08	1501	667	167	74.1	41.7	26.7	18.5	13.6	10.4	8.23	6.67	5.51	4.63	3.75

NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.

2. Thickness refers to the base metal thickness (BMT).

- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
- 5. Capacities are calculated for an equal flange lipped channel using the average flange width.

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#### Part 6: Members with Lips Removed

General

- Table 6.1
   Dimensions & Section Properties
- Table 6.2 Section Properties to Calculate Member Stability
- Table 6.3: Section & Yield Capacities
- Table 6.4: Axial Compression Capacity
- Graph 6.1: Combined Bending & Shear (bending about y-axis)

# Part 6: MEMBERS with LIPS REMOVED

#### GENERAL

When these lipped channel sections are used in frames and trusses, there will be instances where the lips of the sections are removed at the location of the connections. This part of the document provides design tables and graphs which will aid in the design of the unlipoped sections produced by removing the lips. The diagram below illustrates the portion of the section which is removed.

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#### Table 6.1



## **DIMENSIONS & SECTION PROPERTIES**

Lips Removed



	DIMENSIONS							SECTION PROPERTIES								
Designation	Depth	Large Flange Width	Small Flange Width	Thick.	Inside Corner Radius	Co-ord. of Centroid	Mass per metre	Gross Section Area		About x-axis			About	y-axis		
	d	b <sub>f1</sub>	b <sub>f2</sub>	t	r <sub>i</sub>	Xc		Ag	l <sub>x</sub>	Z <sub>x</sub>	r <sub>x</sub>	l <sub>y</sub>	$Z_{\rm yL}$	$Z_{yW}$	ry	
	mm	mm	mm	mm	mm	mm	kg/m	mm <sup>2</sup>	10 <sup>6</sup> mm <sup>4</sup>	10 <sup>3</sup> mm <sup>3</sup>	mm	10 <sup>6</sup> mm <sup>4</sup>	10 <sup>3</sup> mm <sup>3</sup>	10 <sup>3</sup> mm <sup>3</sup>	mm	
89 x 41 x 1.55 LCN-LR - G450	89.0	38.3	36.0	1.55	1.50	9.12	1.92	245	0.296	6.65	34.7	0.0325	1.161	3.56	11.5	
89 x 41 x 1.15 LCN-LR - G500	89.0	38.7	36.4	1.15	1.50	9.10	1.44	184	0.225	5.05	35.0	0.0252	0.889	2.77	11.7	
89 x 41 x 0.95 LCN-LR - G550	89.0	38.9	36.6	0.95	1.50	9.09	1.20	153	0.188	4.22	35.1	0.0213	0.745	2.34	11.8	
89 x 41 x 0.75 LCN-LR - G550	89.0	39.1	36.8	0.75	1.50	9.09	0.952	121	0.150	3.37	35.2	0.0172	0.598	1.90	11.9	

NOTES:

1. Calculations of section properties are in accordance with AS/NZS 4600.

2. Thickness refers to the base metal thickness (BMT).

3. Properties are calculated for an equal flange lipped channel using the average flange width.

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#### Table 6.2



# SECTION PROPERTIES TO CALCULATE MEMBER STABILITY

Lips Removed



	DIMENSIONS								RATIOS PROPERTIES					MATERIAL				
Designation	Depth	Large Flange Width	Small Flange Width	Thick- ness	Inside Corner Radius	Flat Web Depth	Flat Flange Width b	Mass per metre	Web d1/t	Flange b/t	Shear Centre Co-ord.	Polar Rad. of Gyration about S.C.	Mono- Symmetry Constant	Torsion Constant	1	Grade	Yield	Design Tensile Strength
	d	D <sub>f1</sub>	b <sub>f2</sub>	l	r <sub>i</sub>	<i>d</i> <sub>1</sub>	D		<i>u</i> <sub>1</sub> / <i>i</i>	D/L	x <sub>o</sub>	r <sub>o1</sub>	β <sub>y</sub>	J	1 <sub>W</sub>		<sup>7</sup> y	<sup>7</sup> u
	mm	mm	mm	mm	mm	mm	mm	kg/m			mm	mm		mm <sup>4</sup>	10 <sup>6</sup> mm <sup>6</sup>		MPa	MPa
89 x 41 x 1.55 LCN-LR - G450	89.0	38.3	36.0	1.55	1.50	82.9	34.1	1.92	53.5	22.0	21.2	42.3	98.3	196.3	44.0	G450	450	480
89 x 41 x 1.15 LCN-LR - G500	89.0	38.7	36.4	1.15	1.50	83.7	34.9	1.44	72.8	30.3	21.7	42.8	98.9	81.1	34.5	G500	500	520
89 x 41 x 0.95 LCN-LR - G550	89.0	38.9	36.6	0.95	1.50	84.1	35.3	1.20	88.5	37.1	21.9	43.0	99.2	46.0	29.3	G550	550	550
89 x 41 x 0.75 LCN-LR - G550	89.0	39.1	36.8	0.75	1.50	84.5	35.7	0.952	113	47.5	22.1	43.2	99.5	22.7	23.7	G550	495	495

NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.

2. Thickness refers to the base metal thickness (BMT).

3. Steel grades are in accordance with AS 1397.

4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.

5. Properties are calculated for an equal flange lipped channel using the average flange width.

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#### Table 6.3

## **SECTION & YIELD CAPACITIES**

Lips Removed



	Mass	Design Sectior	n Axial Capacities	Design S	ection Moment (	Capacities	Design Yield Moment Capacities (Tension)				
Designation	made	Tension	Compression	about x-axis	about y-axis		about x-axis	about y-axis			
Designation	per m	$\phi_t N_t$	$\phi_c N_s$	$\phi_b M_{sx}$	$\phi_{\sf b} M_{\sf syT}$	$\phi_{\sf b} M_{\sf syW}$	$\phi_{\sf b} M_{\sf sxf}$	$\phi_{\rm b}M_{\rm syfT}$	$\phi_{\sf b} M_{\sf syfW}$		
	kg/m	kN	kN	kNm	kNm	kNm	kNm	kNm	kNm		
89 x 41 x 1.55 LCN-LR - G450	1.92	99.3	61.4	2.01	0.400	0.470	2.69	0.470	1.44		
89 x 41 x 1.15 LCN-LR - G500	1.44	82.8	39.5	1.31	0.265	0.352	2.27	0.400	1.25		
89 x 41 x 0.95 LCN-LR - G550	1.20	75.6	30.2	1.01	0.205	0.277	2.09	0.369	1.16		
89 x 41 x 0.75 LCN-LR - G550	0.952	54.0	18.7	0.629	0.129	0.176	1.50	0.266	0.844		

NOTES:

- 1. Calculations of section capacities are in accordance with AS/NZS 4600.
- 2. Thickness refers to the base metal thickness (BMT).
- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600 Clause 1.5.1.1 where appropriate.
- φ<sub>b</sub>M<sub>syT</sub> and φ<sub>b</sub>M<sub>syW</sub> refer to bending about the y-axis causing compression in the toes and web of the channel respectively.
- 6.  $\phi_b M_{syfT}$  and  $\phi_b M_{syfW}$  are the design yield moment capacities for bending about the y-axis causing tension in the toes and web of the channel respectively.
- 7. All section moment capacities are applicable for unrestrained lengths up to 400 mm. Lips removed WICK \_\_\_\_\_\_ for more than this length is not expected.
- 8. Capacities are calculated for an equal flange channel using the average flange width.



# $t \rightarrow b_{f1}$

# AXIAL COMPRESSION CAPACITY

Table 6.4

 $L_{\text{ex}} = L_{\text{ey}} = L_{\text{ez}}$ Lips Removed



	Mass	Design Axial Compression Capacity, $\phi_c N_c$ (kN)										
Designation	per metre		Effec	tive Length	n (L <sub>e</sub> ) in m	etres						
	kg/m	0.0	0.10	0.20	0.30	0.35	0.40					
89 x 41 x 1.55 LCN-LR - G450	1.92	61.4	61.0	59.9	58.1	56.9	55.6					
89 x 41 x 1.15 LCN-LR - G500	1.44	39.5	39.3	38.5	37.2	36.4	35.5					
89 x 41 x 0.95 LCN-LR - G550	1.20	30.2	30.0	29.3	28.3	27.6	26.9					
89 x 41 x 0.75 LCN-LR - G550	0.952	18.7	18.6	18.3	17.7	17.3	16.9					

#### NOTES:

1. Calculations of section capacities are in accordance with AS/NZS 4600.

- 2. Thickness refers to the base metal thickness (BMT).
- 3. Steel grades are in accordance with AS 1397.
- 4. The design yield stress and design tensile strength are reduced in acccordance with AS/NZS 4600.
- 5. Refer to Graph 3.1 for the limits of the local and distortional design moment capacities.
- 6. The effective length  $L_e = L_{ex} = L_{ey} = L_{ez}$ .
- 7. Capacities are calculated for an equal flange lipped channel using the average flange width.





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bending about y-axis

Lips Removed

Graph 6.1





Web in Compression





Tension

**Toes in Compression** 

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- Table 7.1: Wall stud Design Capacities Unclad
- Table 7.1: Wall stud Design Capacities Clad Both Sides
- Table 7.2: Wall Plate Design Capacities

# Part 7: Wall Framing Design Capacities

#### GENERAL

This part of the Design Capacity tables provide capacities which may be used for the design of the sections as wall studs and wall plates. Three typical wall heights are specified for the wall studs.

The NASH wall stud and plate classifications for both Australia and New Zealand are also included in the tables for each section. These are based on the minimum properties and capacities given in the NASH references.

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## Table 7.1

# WALL STUD DESIGN CAPACITIES

Unclad



	Mass				Design Pro	perties and	Capacities				N/	ASH
Designation	per metre		Lateral	Actions		Compr	ression	Tension	Combined	d Actions	Wal	Stud
Designation	metre	l <sub>x</sub>	$\phi_{\sf b} M_{\sf sx}$	$\phi_{\rm b} M_{\rm bx}$	$\phi_{\rm v} V_{\rm vx}$	$\phi_{\rm c} N_{\rm s}$	$\phi_{\rm c} N_{\rm c}$	$\phi_t N_t$	$\phi_{\sf b}M_{\sf sxf}$	N <sub>ex</sub>	Class	fication
	kg/m	10 <sup>6</sup> mm <sup>4</sup>	kNm	kNm	kN	kN	kN	kN	kNm	kN	Australia	New Zealand
					Stud	Height 2440	mm					
89 x 41 x 1.55 LCN - G450	2.18	0.347	3.16	2.83	30.3	80.4	49.6	86.7	3.16	144	SC	SD
89 x 41 x 1.15 LCN - G500	1.64	0.264	2.56	2.03	15.8	52.3	30.8	70.4	2.67	108	SC	SD
89 x 41 x 0.95 LCN - G550	1.36	0.220	2.01	1.65	8.87	40.2	22.6	61.9	2.45	89.6	SC	SD
89 x 41 x 0.75 LCN - G550	1.08	0.176	1.27	1.12	4.34	25.1	15.0	44.2	1.76	71.1	SB	SB
Stud Height 2740 mm												
89 x 41 x 1.55 LCN - G450	2.18	0.347	3.16	2.83	30.3	80.4	43.5	86.7	3.16	114	SC	SD
89 x 41 x 1.15 LCN - G500	1.64	0.264	2.56	2.03	15.8	52.3	26.9	70.4	2.67	85.6	SC	SD
89 x 41 x 0.95 LCN - G550	1.36	0.220	2.01	1.65	8.9	40.2	19.5	61.9	2.45	71.1	SC	SD
89 x 41 x 0.75 LCN - G550	1.08	0.176	1.27	1.12	4.34	25.1	13.1	44.2	1.76	56.4	SB	SB
					Stud	Height 3040	mm					
89 x 41 x 1.55 LCN - G450	2.18	0.347	3.16	2.83	30.3	80.4	50.5	86.7	3.16	92.7	SC	SD
89 x 41 x 1.15 LCN - G500	1.64	0.264	2.56	2.03	15.8	52.3	31.7	70.4	2.67	69.5	SC	SD
89 x 41 x 0.95 LCN - G550	1.36	0.220	2.01	1.65	8.9	40.2	23.3	61.9	2.45	57.7	SC	SD
89 x 41 x 0.75 LCN - G550	1.08	0.176	1.27	1.12	4.34	25.1	15.4	44.2	1.76	45.8	SB	SB



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#### Wall Stud Design Assumptions

Effective Lengths for Design									
Stud Height (mm)	2440	2740	3040						
No. of Noggings	1	1	2						
L <sub>ex</sub> (mm)	1952	2192	2432						
L <sub>ey</sub> (mm)	976	1096	810						
L <sub>ez</sub> (mm)	976	1096	810						

#### NOTES:

- 1. Noggings are equally spaced.
- 2. Lateral restraint is assumed to be provided by noggings only. Additional lateral restraint provided by cladding is ignored.
- 3. Both flanges of the stud are restrained by the top and bottom plates and the noggings.
- 4. Effective lengths are taken as 80% of the distance between restraints in accordance with NASH Handbook Clause 3.4.2.
- 5. No allowance has been made for holes in the web of the stud.

Symbol	Description
l <sub>x</sub>	second moment of area about the major principal x-axis
$\phi_{c} N_{s}$	design section capacity of a member in compression
$\phi_{\rm c} N_{\rm c}$	design member capacity of a member in compression
$\phi_{\rm b} M_{\rm sx}$	design section moment capacity about the x-axis
$\phi_{\rm b} M_{\rm bx}$	design member moment capacity about the x-axis
$\phi_{\rm b} M_{\rm sxf}$	design yield moment capacity about the x-axis
$\phi_{\rm v} V_{\rm vx}$	design shear capacity of the cross-section perpendicular to the x-axis
N <sub>ex</sub>	elastic buckling load about the major principal x-axis
$\phi_t N_t$	design section capacity of a member in tension
L <sub>ex</sub>	effective length for buckling about the major principal x-axis
L <sub>ey</sub>	effective length for buckling about the minor principal y-axis
L <sub>ez</sub>	effective length for torsional buckling about the longitudinal z-axis

#### References

AS/NZS 4600 Cold-Formed Steel Structures.

NASH Standard (NZ), Residential and Low-Rise Steel Framing, Part 1: Design Criteria.

NASH Standard (Aust.), Residential and Low-Rise Steel Framing, Part 2: Design Solutions.

NASH Handbook (Aust.), Best Practice for Design and Construction of Residential and Low-Rise Steel Framing, Chapter 3.

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Table 7.2

# WALL STUD DESIGN CAPACITIES

Clad Both Sides



	Mass				Design Pro	perties and	Capacities				N/	ASH
Designation	per metre		Lateral	Actions		Compr	ession	Tension	Combine	d Actions	Wall Stud Classification	
Designation	metre	l <sub>x</sub>	$\phi_{\sf b} M_{\sf sx}$	$\phi_{\sf b} M_{\sf bx}$	$\phi_v V_{vx}$	$\phi_{\rm c} N_{\rm s}$	$\phi_{\rm c} N_{\rm c}$	$\phi_t N_t$	$\phi_{\sf b} M_{\sf sxf}$	N <sub>ex</sub>	Classi	fication
	kg/m	10 <sup>6</sup> mm <sup>4</sup>	kNm	kNm	kN	kN	kN	kN	kNm	kN	Australia	New Zealand
					Stud	Height 2440	mm					
89 x 41 x 1.55 LCN - G450	2.18	0.347	3.16	2.83	30.3	80.4	60.7	86.7	3.16	144	SC	SD
89 x 41 x 1.15 LCN - G500	1.64	0.264	2.56	2.03	15.8	52.3	38.7	70.4	2.67	107.9	SC	SD
89 x 41 x 0.95 LCN - G550	1.36	0.220	2.01	1.65	8.87	40.2	29.0	61.9	2.45	89.6	SC	SD
89 x 41 x 0.75 LCN - G550	1.08	0.176	1.27	1.12	4.34	25.1	18.7	44.2	1.76	71.1	SC	SC
					Stud	Height 2740	mm					
89 x 41 x 1.55 LCN - G450	2.18	0.347	3.16	2.83	30.3	80.4	58.0	86.7	3.16	114	SC	SD
89 x 41 x 1.15 LCN - G500	1.64	0.264	2.56	2.03	15.8	52.3	36.9	70.4	2.67	85.6	SC	SD
89 x 41 x 0.95 LCN - G550	1.36	0.220	2.01	1.65	8.9	40.2	27.5	61.9	2.45	71.1	SC	SD
89 x 41 x 0.75 LCN - G550	1.08	0.176	1.27	1.12	4.34	25.1	17.9	44.2	1.76	56.4	SC	SC
					Stud	Height 3040	mm					
89 x 41 x 1.55 LCN - G450	2.18	0.347	3.16	2.83	30.3	80.4	55.0	86.7	3.16	92.7	SC	SD
89 x 41 x 1.15 LCN - G500	1.64	0.264	2.56	2.03	15.8	52.3	34.8	70.4	2.67	69.5	SC	SD
89 x 41 x 0.95 LCN - G550	1.36	0.220	2.01	1.65	8.9	40.2	25.9	61.9	2.45	57.7	SC	SD
89 x 41 x 0.75 LCN - G550	1.08	0.176	1.27	1.12	4.34	25.1	17.0	44.2	1.76	45.8	SC	SC



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#### Wall Stud Design Assumptions

Effective Lengths for Design										
Stud Height (mm)	2440	2740	3040							
No. of Noggings	1	1	2							
L <sub>ex</sub> (mm)	1952	2192	2432							
L <sub>ey</sub> (mm)	600	600	600							
L <sub>ez</sub> (mm)	600	600	600							

#### NOTES:

- 1. Noggings are equally spaced.
- 2. Lateral restraint is assumed to be provided the cladding.
- 3. Both flanges of the stud are restrained by the top and bottom plates, the nogging, and the cladding
- 4. Effective length  $L_{\text{ex}}$  is taken as 80% of the ength of the stud in accordance with NASH Handbook Clause 3.4.2.
- 5. Effective lengths  $L_{ev}$  and  $L_{ez}$  are assumed to be as per the table above.
- 6. No allowance has been made for holes in the web of the stud.

Symbol	Description
I <sub>x</sub>	second moment of area about the major principal x-axis
$\phi_{\rm c} N_{\rm s}$	design section capacity of a member in compression
$\phi_{\rm c} N_{\rm c}$	design member capacity of a member in compression
$\phi_{\rm b} M_{\rm sx}$	design section moment capacity about the x-axis
$\phi_{\rm b} M_{\rm bx}$	design member moment capacity about the x-axis
$\phi_{\sf b} M_{\sf sxf}$	design yield moment capacity about the x-axis
$\phi_{\rm v} V_{\rm vx}$	design shear capacity of the cross-section perpendicular to the x-axis
N <sub>ex</sub>	elastic buckling load about the major principal x-axis
$\phi_t N_t$	design section capacity of a member in tension
L <sub>ex</sub>	effective length for buckling about the major principal x-axis
L <sub>ey</sub>	effective length for buckling about the minor principal y-axis
L <sub>ez</sub>	effective length for torsional buckling about the longitudinal z-axis

#### References

AS/NZS 4600 Cold-Formed Steel Structures.

NASH Standard (NZ), Residential and Low-Rise Steel Framing, Part 1: Design Criteria. NASH Standard (Aust.), Residential and Low-Rise Steel Framing, Part 2: Design Solutions. NASH Handbook (Aust.), Best Practice for Design and Construction of Residential and Low-Rise Steel Framing, Chapter 3.

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#### Table 7.3



# WALL PLATE DESIGN CAPACITIES



	Mass per	Design Properties and Capacities								NASH	
Designation		Full Lipped Channel (at midspan)				Channel Lips Removed (at supports)				Wall Plate	
Designation	metre	l <sub>y</sub>	$\phi_c N_c$	$\phi_{\rm b}  M_{\rm byL}$	$\phi_{\rm b}  M_{\rm byW}$	$\phi_c N_s$	$\phi_{\rm b} M_{\rm syT}$	$\phi_{\rm b}M_{\rm syW}$	$\phi_v V_{vy}$	Classification	
	kg/m	10 <sup>6</sup> mm <sup>4</sup>	kN	kNm	kNm	kN	kNm	kNm	kN	Australia	New Zealand
89 x 41 x 1.55 LCN - G450	2.18	0.0584	68.6	0.804	0.856	61.4	0.400	0.470	27.4	PC	PD
89 x 41 x 1.15 LCN - G500	1.64	0.0450	44.1	0.590	0.579	39.5	0.265	0.352	23.1	PB	PC
89 x 41 x 0.95 LCN - G550	1.36	0.0378	33.4	0.486	0.509	30.2	0.205	0.277	21.2	PB	PC
89 x 41 x 0.75 LCN - G550	1.08	0.0304	21.2	0.345	0.287	18.7	0.129	0.176	14.9	PA	PA

NOTES:

1. The capacities for the full lipped channels are based on an effective length  $L_e = 0.6$  m.

2. The capacities of channels with lips removed are section capacities.

3. No allowance has been made for holes in the web of the plate in the determination of  $I_{y}$ .

4. The NASH Classifications are based on the capacities of the full lipped channels.

5. The second moment of area  $I_{\rm v}$  for the full lipped channel is used for the NASH Australia classification.

	Symbol	Description
	l <sub>y</sub>	second moment of area about the minor principal y-axis
	$\phi_{\rm c} N_{\rm s}$	design section capacity of a member in compression
	$\phi_{\rm c} N_{\rm c}$	design member capacity of a member in compression
ı.	$\phi_{\sf b}  M_{\sf byL}$	design member moment capacity about the y-axis (lips in compression)
	$\phi_{\rm b} M_{\rm byW}$	design member moment capacity about the y-axis (web in compression)
wi	$\phi_{\sf b} M_{\sf syT}$	design section moment capacity about the y-axis (toes in compression)
	$\phi_{\sf b} M_{\sf syW}$	design section moment capacity about the y-axis (web in compression
	$\phi_{v} V_{vy}$	design shear capacity of the cross-section perpendicular to the y-axis
	L <sub>e</sub>	effective length ( $L_{ex} = L_{ey} = L_{ez}$ )



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# Appendix A: SIGNATURE CURVES

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#### GENERAL

This appendix provides the signature curves for each of the sections contained in these Design Capacity Tables. The signature curves were produced in the Thin-Wall buckling analysis program developed by The University of Sydney, and form the basis of design using the Direct Strength Method (DSM). They are included here to provide a clear picture of the buckling behaviour of the sections under the following loading conditions:

axial compression

bending about the x-axis

bending about the y-axis (lips in compression)

bending about the y-axis (web in compression)



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DESIGN CAPACITY TABLES for 89 x 41 Lipped Channels - Nestable to AS/NZS 4600 Version 02 • January 2019